Hydrogeological Assessment Report -245 Church Street, Penetanguishene, ON



November 15, 2022

Prepared for: Koenig Developments Ltd.

Cambium Reference: 13237-001

CAMBIUM INC.

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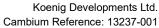
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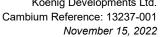
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1.0 Introduction

Cambium Inc. (Cambium) was retained by Koenig Developments Ltd. (the client) to complete a hydrogeological assessment of the property located at 245 Church Street, Town of Penetanguishene, Ontario (herein referred to as Site).

The Site is approximately 5.30 hectares (2.13 acres) in size and is currently a vacant land covered with trees and bushes. Cambium understands that the hydrogeological investigation is required in support of the proposed residential development at the Site.

It is noted that this scale of development meets the definition of "Major Development" per the Lake Simcoe Protection Plan (LSPP), and the South Georgian Bay Lake Simcoe Source Protection Plan (SGBSPP).

1.1 Scope of Work

This hydrogeological investigation was conducted with the following tasks:

- Review of available background information: a review of available geological and hydrogeological information for the site and surrounding areas and the previous investigation reports completed for the Site, was conducted to provide background information to allow for characterization of the Site's soil and groundwater conditions.
- **Detailed site inspection**: an inspection of the Site was completed to review existing site conditions including identification of any hydrogeological features such as significant areas of potential groundwater recharge or areas of groundwater discharge.
- **Measurement of groundwater levels:** groundwater levels were measured in the existing monitoring wells to establish and/or confirm the general groundwater flow condition and elevations.
- Physical Laboratory Soil Testing: results of soil sample testing completed will be utilized to characterize the infiltration rate of the shallow surficial soils (i.e., within approximately 0.5 mbgs). This will help with the design and placement of Low Impact Development (LID) measures, if any across the Site.





- Water Balance (Preliminary): a preliminary water balance study was completed for the
 pre-development and the proposed post-development using the Thornthwaite-Mather
 approach and utilizing the climatic data obtained from Environment Canada.
- Report Preparation: a hydrogeological report was prepared presenting the results, findings, and recommendations of this investigation.

It should be noted that Cambium was also retained for a geotechnical investigation (Cambium, 2022a). The data or information obtained in the current and former investigations has been incorporated into this hydrogeological investigation report.

1.2 Site Description and Site Development

The total area of the property is approximately 5.30 hectares (2.13 acres) in size and the Site is bound to the west by Church Street, Oxley Drive to the east, residential development to the north and scattered residential dwellings to the south. It is proposed that the Site is to be developed into a residential complex consisting of single detached dwellings, row house dwellings, and double duplex dwellings totalling to 32 units along with driveways, parking areas and roadways. Water and wastewater services are being provided by the Town.

The regional location of the Site is outlined on Figure 1, the property and surrounding areas outlined on Figure 2, and the proposed development plan is included in Appendix A.



2.0 **Environmental Features**

To assess environmental features, databases maintained by the Ministry of Natural Resources and Forestry (MNRF), the Ministry of Environment, Conservation and Parks (MECP), and Nottawasaga Valley Conservation Authority (NVCA) were reviewed.

A review of background information indicates the Site is situated within the South Georgian Bay-Lake Simcoe (SGBLS) Source Protection Region, under Severn Sound Source Protection Authority. The Property is designated as Neighborhood Area on Schedule A Land Use Structure per Town of Penetanguishene Official Plan and is within a Significant Groundwater Recharge Area (SGRA) and a Wellhead Protection Area Q1 and Q2 related to groundwater recharge management (Appendix A).

The Site is not situated in NVCA regulated areas per Ont. Reg. 172/06. Therefore, development restrictions do not apply to the proposed development Site, in its entirety.

Available mapping indicates no significant wetlands or woodlands are situated on the Site and a review of the Ministry of Natural Resources and Forestry's (MNRF) Natural Heritage System database further indicates the Site does not have any Areas of Environmental Significance or Areas of Natural and Scientific Interests (ANSI).



Physical Setting 3.0

Topography and Drainage

The Site is located on a peninsula within Severn Sound, in the southeastern portion of Georgian Bay. Shoreline is situated approximately 850 m to the west (Penetang Harbour). Based on the topographic survey completed by RS Surveying Limited, dated October 7, 2022 (Appendix A) of the Site, the property has a topographic high of approximately 228.42 m above sea level (masl) in the west portion of the Site sloping to the lowest elevation of approximately 222.51 masl in the mid-central part of the Site.

3.2 Physiography

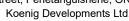
The Site is located in the physiographic region known as Simcoe Uplands. The uplands are comprised of a series of broad, rolling, till plains separated by steep-sided flat-floored valleys. Boulder pavement, sand, and silt appear at surface in the Penetang Peninsula as it was at one time submerged by the glacial Lake Algonquin. Till in the area consists of gritty loam derived from Pre-Cambrian rock. (Chapman & Putnam, 1984).

3.3 Overburden Geology

According to Miscellaneous Release – Data 128 from the Ontario Geological Survey (Ontario Geological Survey, 2010), the Site is underlain primarily by till (stone-poor, sandy silt to silty sand textured till). Coarse-textured glaciolacustrine deposits (sand, gravel, minor silt, and clay), are identified in the majority of the property area.

3.4 Bedrock Geology

According to Miscellaneous Release – Data 219 from the Ontario Geological Survey (Armstrong, D.K. and Dodge, J.E.P., 2007), the Site is underlain by limestone bedrock of the Gull River Formation (Middle Ordovician Simcoe Group rocks). This formation is subdivided into three members. The lower member is characterized by grey to greenish grey finecrystalline dolomitic limestones and calcareous dolostones up to 15 m thick. Light grey to white microcrystalline limestone up to 9m thick comprises the middle member, and the upper





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member is identified as grey, micro- to fine-crystalline limestone up to 3 m thick. (Ontario Geological Survey, 1989).



4.0 MECP Well Records Assessment

Cambium accessed the Ministry of the Environment Conservation and Parks (MECP) Water Well Information System (WWIS) to review water well records within 500 m of the Site.

There were sixteen (16) water well records found within approximately 500 m of the Site. Of the well records, one drilled well was installed in bedrock (Well Record#5716422) has encountered a bedrock at a depth of about 71 m, which was installed as a test hole by the MECP. Rest of the wells were all overburden wells installed from 9.1 mbgs to 87.2 mbgs. The boreholes were installed between the years 1965 and 1996. Deepest borehole (Well#5732671) drilled to a depth of 87.2 mbgs, did not encounter any bedrock. A summary of the depths, static water levels, and pumping rate are shown in Table 1 and the well records have been included as Appendix B.

Table 1 Summary of Surrounding Water Well Record Information

Well Type		Depth (mbgs)	Static Water Level (mbgs)	Recommended Pumping Rate (L/min)
Bedrock Count = 1	Maximum	71.0	38.1	12
	Maximum	9.1	6.3	4
Overburden Count =15	Minimum	87.2	3.0	18
10	Average	41.5	15.8	8

A summary of the information outlined in the well records is provided below:

- Of the records analyzed, all the wells encountered fresh groundwater.
- Overburden was reported as a layer of predominantly sand with some gravel and silt overlying the bedrock (limestone).
- Based on well yields, it is indicated the presence of productive wells in the area.



Borehole Drilling and Monitoring Well Installation

5.1 Borehole Investigation

Cambium completed a geotechnical investigation at the Site on July 21, 2021, to assess the

subsurface conditions. A total of four boreholes, designated as BH101-21 through BH104-21,

were advanced to a depth of 6.6 m below ground surface (mbgs). Borehole locations are

appended as Figure 4. Borehole logs are included in Appendix C.

During the site investigation, three monitoring well was installed in boreholes BH102-21, BH103-

21 and BH104-21 and the groundwater level was measured on a subsequent groundwater

monitoring trips starting from August 3, 2022 to July 6, 2022.

A summary of lithological details is presented below.

Topsoil

A layer of black topsoil with some organics including sand and some silt was observed at the

surface of all boreholes throughout the Site. The thickness of the topsoil ranged between 0.01

m and 0.40 m

Sand

Beneath the topsoil in boreholes BH101-21, BH102-21 and BH104-21, a layer of sand with

varying amounts of gravel, silt and clay was encountered. The material was brown to grey in

colour and extended to 1.5 mbgs in BH101-21, 4.6 mbgs in BH102-21 and the termination depth

of 6.6 mbgs in BH104-21.

Silty Sand and Sandy Silt

Beneath the sand material found in boreholes BH101-21 and BH102-21, a silty sand material

was encountered and extended to the termination depth of 6.6 mbgs. The material was grey in

colour and contained varying amounts of gravel and trace amounts of clay.



Sand and Silt

Below the surficial topsoil layer in borehole BH103-21, a layer of sand and silt material was encountered and extended to the termination depth of 6.6 mbgs. The sand and silt material were brown to grey in colour and contained trace amounts of gravel.

Bedrock

Bedrock was not encountered during this geotechnical investigation. Drilling was terminated at depths of 6.6 mbgs, in native soils.

5.2 Monitoring Well Installation Details

Table 2 below provides all the construction details of monitoring well installation in three of the boreholes.

Table 2 Monitoring Well Installation Details

Monitoring	Termination	Ground Elevation	Screen Details	
Well	Depth (mbgs)	(masl)	Screen Top (masl)	Screen Bottom (masl)
BH102-21	6.6	224.67	221.57	218.57
BH103-21	6.6	223.86	220.76	217.76
BH104-21	6.6	222.65	219.55	216.55

5.3 Long-Term Groundwater Monitoring

As part of hydrogeological investigation, long-term stabilized water level monitoring was completed for 12 months. Groundwater levels were measured between August of 2021 and July of 2022.

Groundwater levels for the entire monitoring period are presented in Table 3 below.

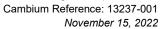




Table 3 Measured Groundwater Levels

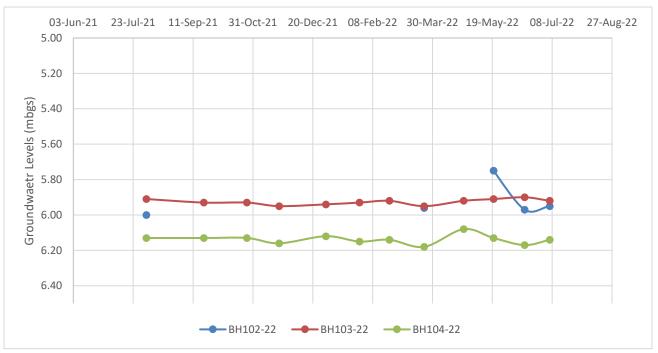
Date	Borehole	Ground Elevation (masl)	Water Level Depth (mbgs)	Water Level Elevation (masl)
	BH102-21	224.67	6.0	218.67
August 3, 2021	BH103-21	223.86	5.91	217.95
	BH104-21	222.65	6.13	216.52
	BH102-21	224.67	Dry	-
September 20, 2021	BH103-21	223.86	5.93	217.93
	BH104-21	222.65	6.13	216.52
	BH102-21	224.67	Dry	-
October 26, 2021	BH103-21	223.86	5.93	2
	BH104-21	222.65	6.13	216.52
	BH102-21	224.67	Dry	-
November 22, 2021	BH103-21	223.86	5.94	217.92
	BH104-21	222.65	6.16	216.49
	BH102-21	224.67	Dry	-
December 21, 2021	BH103-21	223.86	5.94	217.92
	BH104-21	222.65	5.92	216.73
	BH102-21	224.67	Dry	-
January 28, 2022	BH103-21	223.86	5.93	217.93
	BH104-21	222.65	6.15	216.50
	BH102-21	224.67	Dry	-
February 22, 2022	BH103-21	223.86	5.92	217.93
	BH104-21	222.65	6.14	216.51
	BH102-21	224.67	5.96	218.71
March 23, 2022	BH103-21	223.86	5.95	217.91
	BH104-21	222.65	6.18	216.47
	BH102-21	224.67	Dry	-
April 25, 2022	BH103-21	223.86	5.92	217.94
	BH104-21	222.65	6.08	216.57
	BH102-21	224.67	5.75	218.92
May 20, 2022	BH103-21	223.86	5.91	217.95
	BH104-21	222.65	6.13	216.52
luno 15, 2022	BH102-21	224.67	5.97	218.70
June 15, 2022	BH103-21	223.86	5.9	217.96



Date	Borehole	Ground Elevation (masl)	Water Level Depth (mbgs)	Water Level Elevation (masl)
	BH104-21	222.65	6.17	216.48
	BH102-21	224.67	5.95	218.72
June 15, 2022	BH103-21	223.86	5.92	217.94
	BH104-21	222.65	6.14	216.51

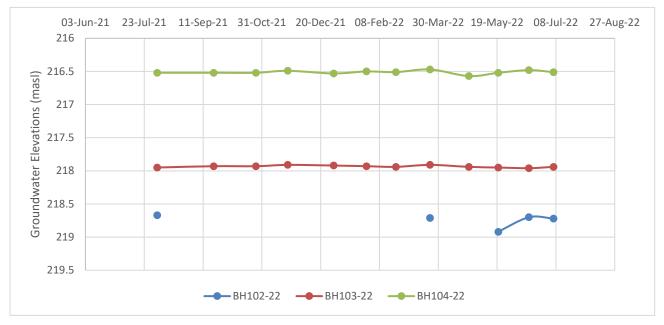
All the groundwater monitoring data is presented below in Embedded Figure 1 and Embedded Figure 2.

Embedded Figure 1 Depth to Groundwater Levels (mbgs)









As presented above, the spring measured groundwater levels in the monitoring wells ranged in depth from 5.75 mbgs to 6.18 mbgs, and the elevations ranged from 216.47 masl to 218.92 masl. As per the long-term water level monitoring, BH102-21, has witnessed water levels only in the spring and was dry rest of the year. The seasonal high-water level of 5.75 mbgs was recorded in the month of May 2022 with the corresponding highest water table elevation at 218.92 masl.

5.4 Groundwater Flow Direction

Based on the groundwater elevation data obtained from the monitoring event (May 20, 2022), a site-specific groundwater elevation contour map was prepared to present the groundwater flow direction across the Site. As shown in Figure 5, the groundwater flow direction was found to be east and southeast following the local surficial drainage.

5.5 Physical Laboratory Testing

Physical laboratory testing, including five (5) sieve and hydrometer analyses (LS-702, 705) was completed on selected soil samples (BH101-21, BH102-21, BH103-21 and BH104-21) to



confirm textural classification and to estimate percolation rates of the native soils. Results are presented in Appendix D and details of the grain-size analysis are presented in Table 4 below.

Based on sieve analysis data, the shallow soil samples (0.6 to 2.0 mbgs) mostly consist of silty sand with trace to some clay and gravel, while the deeper (2.3 to 5.0 mbgs) native soils were predominantly sandy with trace silt and gravel.

Table 4 Particle Size Distribution

ВН	Depth (mbgs)	Description	% Gravel	% Sand	% Silt	% Clay	Percolation Times (min/cm)
BH101- 21 SS3	1.5 – 2.0 m	Silty Sand, some Clay, trace Gravel	7	68	25		14
BH102- 21 SS2	0.6 - 1.2 m	Silty Sand trace Clay and Gravel	4	80	15	4	12
BH102- 21 SS6	4.6 – 5.0 m	Silty Sand, some Gravel, trace Clay	11	62	24	3	14
BH103- 21 SS2	0.6 – 1.2 m	Silty Sand, trace Gravel	3	62	35		20
BH104- 21 SS4	2.3 – 2.7 m	Sand, trace Silt and Gravel	4	87	9		6

The soil percolation rates ranged between as low as 20 min/cm and as high as 6 min/cm. The geometric mean of the percolation rate was estimated at about 12 min/cm, indicating the presence of relatively high transmissive soils with good drainage capacity.

5.6 In-Situ Hydraulic Conductivity Tests

The in-situ hydraulic conductivity tests could not be conducted as the wells were either dry or have insufficient water column to conduct either a falling head test or rising head tests.

Therefore, the hydraulic conductivity (k-value) of the native soils could not be estimated.



6.0 Construction Dewatering Assessment

Construction dewatering is intended to lower the groundwater levels in the excavation area in order to ensure a dry working condition for the construction operations at the Site.

The requirements for construction dewatering generally depend on the Site's soil and groundwater conditions including soil type, soil permeability or hydraulic conductivity, local groundwater levels, and the design of the proposed works, such as the foundation and/or basement elevation, as well as the size of proposed structure / excavation.

The proposed residential development could possibly include a basement under the proposed single detached dwellings, row house dwellings, and double duplex dwellings and accordingly, the basement might extend to a depth of about 3.5 m (10.5 ft.) below the existing grade. At the time of this report, no details regarding the finished floor elevation (FFE) or grade elevations were available.

Based on the groundwater monitoring data, the spring measured groundwater levels in the monitoring wells ranged in depth from 5.75 mbgs to 6.18 mbgs, and the elevations ranged from 216.47 masl to 218.92 masl. Since, the depth to water level is more than 2 m below the bottom elevations of the likely basements, no dewatering either short or long term would be required for the proposed development under the existing ground conditions.



7.0 Water Balance Assessment

Based on the Thornthwaite and Mather methodology (Thornthwaite & Mather, 1957), the water balance is an accounting of water in the hydrologic cycle. Precipitation (P) falls as rain and snow. It can run off towards lakes and streams (R), infiltrate to the groundwater table (I), or evaporate from ground or evapotranspiration by vegetation (ET). When long-term average values of P, R, I, and ET are used, there is minimal or no net change to groundwater storage (Δ S).

The annual water budget can be expressed as:

 $P = ET + R + I + \Delta S$

Where:

P = Precipitation (mm/year)

ET = Evapotranspiration (mm/year)

R = Run-off (mm/year)

I = Infiltration (mm/year)

 ΔS = Change in groundwater storage (taken as zero) (mm/year)

It is noted that the water balance described herein does not account for catchment areas that extend off-site. The calculations compare the pre- and post-development water balance changes within the Site boundaries.

The pre-development portion of the Site is mainly a vacant land.

It is understood that the proposed development consists of single detached dwellings, row house dwellings, and double duplex dwellings totalling to 32 units along with driveways, parking areas and roadways.

Based on the available design information, the development area at the Site can be generally categorized into three (3) types as paved area, roof area, and landscape areas. Based on the development concept plan (Appendix A) the roof, landscape and paved were estimated and a summary of the surface areas of the development is listed in Table 5.



Table 5 Pre- and Post-Development Site Statistics

Type of Land Coverage	Pre-Development Areas (m²)	Post-Development Areas (m²)
Paved Area	-	10,600
Building Roof Area	-	9,525
Landscape/Vegetated Area	53,000	32,875
Total (m ²)	53,000	53,000

Supporting information referenced herein (including detailed water balance calculations) is attached in Appendix E.

7.1 Water Surplus

Water surplus is calculated by determining the difference between precipitation and evapotranspiration (changes in soil water storage was assumed to be negligible over the course of a year). The volume of water surplus is further sub-divided into portions that infiltrate the on-site soils and that are directed off-site as runoff.

The climatic data including monthly average temperature and precipitation were obtained from Environment Canada, for Midland weather station (Climate Identifier: 6115127) located about 6 km distance from the Site. Data was available for a period of 29 years from 1981 to 2010. Accordingly, the average annual evapotranspiration was estimated to be about 547 mm/annum using the USGS Thornthwaite Monthly Water Balance methodology (Appendix E), and the average annual precipitation was recorded to be 1,041 mm/annum. The water surplus of the Site was calculated to be 494 mm/year.

Evapotranspiration does not occur from structures, paved areas, or hard gravel surfaces. It was assumed that 10% of precipitation falling on these surfaces is lost directly to evaporation. The remaining depth (i.e., 90% of precipitation) was considered surplus and converted to infiltration and/or runoff.

7.2 Infiltration Rates

The volume of surplus water that infiltrates through pervious surfaces on-site was determined by applying an infiltration factor to the surplus depth. The surplus water that does not infiltrate



into pervious surfaces will leave the Site as surface water runoff. The infiltration factor varies from 0 to 1 and is estimated based on topography, soils, and vegetation cover as per the *Stormwater Management Planning and Design Manual* (Ministry of the Environment, 2003).

The rate of infiltration at a site is expected to vary, based on a number of factors to be considered in any infiltration model. To partition the available water surpluses into infiltration and surface run-off, the Ministry of Environment, Conservation and Parks (MECP) infiltration factor was used. The MECP Storm Water Management Planning and Design Manual (2003) methodology for calculating total infiltration based on topography, soil type and land cover was used, and a corresponding run-off component was calculated for the soil moisture storage conditions.

The Site is relatively a gently undulating to sloping topography, and based on the results of the borehole investigation, the subsurface conditions at the Site predominantly consist of sand with silt and gravel extending to a depth of approximately 6.0 mbgs.

The calculation of infiltration and runoff in the stages of pre-development and postdevelopment is provided in Appendix E, and are presented in Table 6 through Table 9 below.

7.3 Pre-Development Water Balance

The water balance for the existing conditions of the Site is summarized in Table 6. The predevelopment infiltration rate was calculated to be 18,327 m³/yr and the runoff rate was 7,855 m³/yr.

Table 6 Pre-Development Water Balance

Land Use		Area (m²)	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run- off (m³)
Impervious	Paved Area	-	-	-	-	-
Areas	Roof Area	-	-	-	-	-
Pervious Areas	Landscape Area	53,000	55,173	28,991	18,327	7,855
		53,000	55,173	28,991	18,327	7,855

Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.



7.4 Post-Development Water Balance

The post-development water balance is summarized in Table 7. The post-development infiltration rate was estimated at 11,368 m³/yr and the runoff rate was at 23,727 m³/yr.

Table 7 Post-Development Water Balance

Land	Use	Area (m²)	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run- off (m³)
Impervious	Paved Area	10,600	11,035	1,103	-	9,931
Areas	Roof Area	9,525	9,916	992	-	8,924
Pervious Areas	Landscape Area	32,875	34,223	17,983	11,368	4,872
		53,000	55,173	20,078	11,368	23,727

Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.

7.5 Water Balance Comparison

The water balances of the pre-development and post-development scenarios are summarized below in Table 8.

Table 8 Water Balance Comparison

	Precipitation (m³)	Evapotranspiration (m3)	Infiltration (m³)	Run- off (m³)
Pre-Development	55,173	28,991	18,327	7,855
Post-Development	55,173	20,078	11,368	23,727
Change in Volume	-	-8,913	-6,959	15,873
Change in %	-	-31	-38	202

Based on the above, there is an infiltration deficit of about 6,959 m³/year compared to the predevelopment infiltration. The runoff rate upon development of the Site was increased by about 15,873 m³/year.



Table 9 Requirement of Infiltration from Roof Run-off

Volume of Pre-Development Infiltration (m³/annum)	18,327
Volume of Post-Development Infiltration (m³/annum)	11,368
Deficit from Pre to Post Development Infiltration (m³/annum)	6,959
% of Roof Runoff required to match the pre-development Infiltration	78

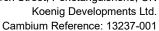
Based on the above calculations, a summary of the water balance could be provided as follows:

- 1. There is a net increase in run-off at the Site of about 15,873 m³/annum, from 7,585 m³/annum to 23,727 m³/annum. This increase is a result of the development of the Site with more impervious areas such as roof and paved areas and decrease in pervious areas.
- 2. Post-development landscape area was decreased by about 20,125 m², when compared to the pre-development landscape, causing less infiltration and more run-off across the Site.
- 3. Without implementing any mitigation measures, there is a net deficit of about 6,959 m³ /annum in the post-development infiltration on a yearly basis.
- 4. Based on the estimation, considering the diversion of about 78% of the general roof water for infiltration, the proposed development would maintain the pre-development infiltration after the development. Therefore, Cambium would recommend the design and implementation of Low Impact Development (LID) measures at the Site.

7.6 Discussions on LID Measures

It is known that low impact development (LID) practices have received increasing attention as these strategies attempt to capture the runoff and mimic the natural hydrologic cycle.

In general, there are two primary categories of LIDs. The first promotes the infiltration of Stormwater close to the source. These infiltration type LIDs are preferred when hydrogeological and physical conditions are optimal and allow for their emplacement. The proposed development does not include a stormwater management pond to improve water quality and enhance the lost infiltration due to the Site development with paved and roof areas. Therefore, the second option which captures and slowly releases the water to the ground





water system through the process of storage and filtration by infiltration LIDs should be considered.

Roof downspout disconnection is an option available for the Site. Considering a conservative run-off capture rate estimate of 25%, the total volume of roof run-off water available for infiltration is approximately 2,230 m³/yr, leaving approximately 4,725 m³/yr still to be compensated at the Site. Roof downspouts should only be disconnected where the minimum depth to the seasonally high water table is at least 1 m below the surface. As relatively deep water table conditions are present at the Site, this LID measurement will be feasible. Additional LID measures, such as infiltration trenches, infiltration galleries, soak-away pits etc., can be utilized to enhance infiltration in addition to roof downspout disconnects.

As there is an infiltration deficit in the post-development scenario, Cambium does recommend implementing any suitable LID measures, along with Best Management Practices (BMPs) to enhance and compensate the infiltration deficit. However, Cambium is not providing any design of LID facilities, it would be beneficial to consult with design engineers for the LID design recommendations.



8.0 Source Water Protection And Risk Management

As per the MECP Source Protection Information Atlas (SPIA) and SBLP Source Protection Plan (SPP), the western half of the Subject Site is located within a Significant Groundwater Recharge Area (SGRA) and the entire Site is within a Wellhead Protection Area Q1 and Q2 related groundwater recharge management (Appendix A).

SGRA

SGRAs exist in areas where water from surface more easily infiltrates the ground to recharge an aquifer that is used for municipal or other drinking water supplies. Under the Clean Water Act, 2006, a SGRA helps maintain the water level in an aguifer that supplies drinking water (including to private wells) and has higher than average recharge comparatively across the Source Protection Area.

In the present development scenario, as the development will create more impervious areas across the Site causing a reduction in infiltration, we recommend implementing the LID measures where practicable. The proposed development does not involve any long-term dewatering and therefore, a potential reduction to ground water supplies was not expected.

WHPA Q1/Q2

As per Section 58 of the SBLP SPP, a risk management plan should ensure that the threat to drinking water ceases to be significant. A climate based water balance assessment was completed for the pre- and post-development scenarios for the Site as described in Section 7. A climate based water balance assessment is the first step to identify the post-development infiltration deficit and then utilize the Best Management Practices (BMPs) to minimize any infiltration deficit.

Accordingly, as per the water balance assessment completed above, it was estimated that there is a net infiltration deficit between the pre- and development scenarios in the order of 6,959 m³/annum.

The preferred solution for recharge management is always for the post-development infiltration deficit to be mitigated during the development process. In the present scenario, due to deep



water table conditions and the presence highly permeable sandy soils at the Site, we recommend exploring all the LID measures such as infiltration trenches, infiltration galleries or other suitable measures to encourage the roof water run-off infiltration in order to mitigate the estimated infiltration deficit.

The Site will be under municipal sewage and water services and as such the proposed development is not expected to cause any groundwater contamination by nitrates.



9.0 Assessment of Potential Impacts

Based on the information available, the residential development at the Site may likely have

one-level basement and based on water levels there is no construction dewatering, either

short-term or long-term was anticipated at the Site. The potential impacts due to the Site

development were assessed as below.

9.1 Natural Features

As discussed, no natural features such as wetlands, woodlands or creeks are located on the

Site and therefore, there should be no impacts on the local natural features, due to the Site

development. Also, the Site is not located in NVCA regulation areas and as per the O. Reg.

172/06, regulation limits prescribed by the Conservation Authority are not applicable to the Site

development.

9.2 Water Supply Wells near the Site

Given that no dewatering will be required for completion of the proposed development, impacts

on the local water wells (private or public), if any will not be anticipated to be associated with

the dewatering activity.

9.3 Considerations on Drinking Water Vulnerability

Based on the MECP Source Protection Information Atlas, the Site is situated partly within

SGRA and entirely in WHPA Q1/Q2 and therefore, best management practices and other

measures described in Section 8 should be followed in order to reduce the qualitative and

quantitative impacts on the local groundwater regime.



10.0 Conclusions and Recommendations

Cambium Inc. (Cambium) was retained by Koenig Developments Ltd. (the Client) to complete a hydrogeological assessment of the property located at 245 Church Street, Town of Penetanguishene, ON (the Site).

Subject Property is situated within the Severn Sound watershed under the jurisdiction of the NVCA Source Protection Area and no wetlands or woodlands or creeks are situated on the Site.

The measured groundwater levels in the monitoring wells ranged in depth from 5.75 mbgs to 6.18 mbgs, and the elevations ranged from 216.47 masl to 218.92 masl.

As per the long-term water level monitoring, the spring seasonal high water level of 5.75 mbgs was recorded in the month of May 2022 and water table elevation was at 218.92 masl.

Groundwater flow direction was found to be east and southeast following the local surficial drainage.

Based on the water table elevations and excavation depths for the likely one level basement, temporary short-term groundwater control (construction dewatering) will not be required. Also, the one level basement slab elevation would be well above the water table elevation and therefore, long-term sub-drain drainage was not expected at the Site.

The conceptual water balance indicates that there will be an infiltration deficit of 6,959 m³ /annum upon the development of the Site. About 78% of the runoff generated from roof surfaces can account for the infiltration deficit if it is captured and re-infiltrated.

The Site will be under municipal sewage and water services and as such the proposed development is not expected to cause any groundwater contamination by nitrates.

As the Site is situated within a SGRA and WHPA Q1/Q2, the preferred solution for recharge management is always for the post-development infiltration deficit to be mitigated during the development process. In the present scenario, due to deep water table conditions and the presence of highly permeable sandy soils at the Site, we recommend exploring all the possible



LID measures and adhering to the best management practices in order to protect the local groundwater supplies.

Respectfully submitted,

Cambium Inc.

Nicole Heikoop, M.Sc., GIT Technologist

Sudhakar Kurli, M.Sc., P.Geo. Project Manager/Hydrogeologist

Skurli

NMH/SK

P:\13200 to 13299\13237-001 Schuren Sriskandarajah - Water Balance and Hydrogeological Assessment - 245 Church St



11.0 References

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Thornthwaite, C., & Mather, J. (1957). Instructions and tables for computing potential evapotranspiration and the water balance. Centerton, N.J.: Laboratory of Climatology, Publications in Climatology, v. 10, no. 3, p. 185-311.

Hydrogeological Assessment Report - 245 Church Street, Penetanguishene, ON Koenig Developments Ltd.

Cambium Reference: 13237-001

November 15, 2022

12.0 Standard Limitations

Limited Warranty

In performing work on behalf of a client, Cambium relies on its client to provide instructions on the scope of its retainer and, on that basis, Cambium determines the precise nature of the work to be performed. Cambium undertakes all work in accordance with applicable accepted industry practices and standards. Unless required under local laws, other than as expressly stated herein, no other warranties or conditions, either expressed or implied, are made regarding the services, work or reports provided.

Reliance on Materials and Information

The findings and results presented in reports prepared by Cambium are based on the materials and information provided by the client to Cambium and on the facts, conditions and circumstances encountered by Cambium during the performance of the work requested by the client. In formulating its findings and results into a report, Cambium assumes that the information and materials provided by the client or obtained by Cambium from the client or otherwise are factual, accurate and represent a true depiction of the circumstances that exist. Cambium relies on its client to inform Cambium if there are changes to any such information and materials. Cambium does not review, analyze or attempt to verify the accuracy or completeness of the information or materials provided, or circumstances encountered, other than in accordance with applicable accepted industry practice. Cambium will not be responsible for matters arising from incomplete, incorrect or misleading information or from facts or circumstances that are not fully disclosed to or that are concealed from Cambium during the provision of services, work or reports.

Facts, conditions, information and circumstances may vary with time and locations and Cambium's work is based on a review of such matters as they existed at the particular time and location indicated in its reports. No assurance is made by Cambium that the facts, conditions, information, circumstances or any underlying assumptions made by Cambium in connection with the work performed will not change after the work is completed and a report is submitted. If any such changes occur or additional information is obtained, Cambium should be advised and requested to consider if the changes or additional information affect its findings or results.

When preparing reports, Cambium considers applicable legislation, regulations, governmental guidelines and policies to the extent they are within its knowledge, but Cambium is not qualified to advise with respect to legal matters. The presentation of information regarding applicable legislation, regulations, governmental guidelines and policies is for information only and is not intended to and should not be interpreted as constituting a legal opinion concerning the work completed or conditions outlined in a report. All legal matters should be reviewed and considered by an appropriately qualified legal practitioner.

Site Assessments

A site assessment is created using data and information collected during the investigation of a site and based on conditions encountered at the time and particular locations at which fieldwork is conducted. The information, sample results and data collected represent the conditions only at the specific times at which and at those specific locations from which the information, samples and data were obtained and the information, sample results and data may vary at other locations and times. To the extent that Cambium's work or report considers any locations or times other than those from which information, sample results and data was specifically received, the work or report is based on a reasonable extrapolation from such information, sample results and data but the actual conditions encountered may vary from those extrapolations.

Only conditions at the site and locations chosen for study by the client are evaluated; no adjacent or other properties are evaluated unless specifically requested by the client. Any physical or other aspects of the site chosen for study by the client, or any other matter not specifically addressed in a report prepared by Cambium, are beyond the scope of the work performed by Cambium and such matters have not been investigated or addressed.

Reliance

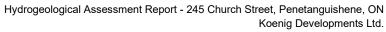
Cambium's services, work and reports may be relied on by the client and its corporate directors and officers, employees, and professional advisors. Cambium is not responsible for the use of its work or reports by any other party, or for the reliance on, or for any decision which is made by any party using the services or work performed by or a report prepared by Cambium without Cambium's express written consent. Any party that relies on services or work performed by Cambium or a report prepared by Cambium without Cambium's express written consent, does so at its own risk. No report of Cambium may be disclosed or referred to in any public document without Cambium's express prior written consent. Cambium specifically disclaims any liability or responsibility to any such party for any loss, damage, expense, fine, penalty or other such thing which may arise or result from the use of any information, recommendation or other matter arising from the services, work or reports provided by Cambium.

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Potential liability to the client arising out of the report is limited to the amount of Cambium's professional liability insurance coverage. Cambium shall only be liable for direct damages to the extent caused by Cambium's negligence and/or breach of contract. Cambium shall not be liable for consequential damages.

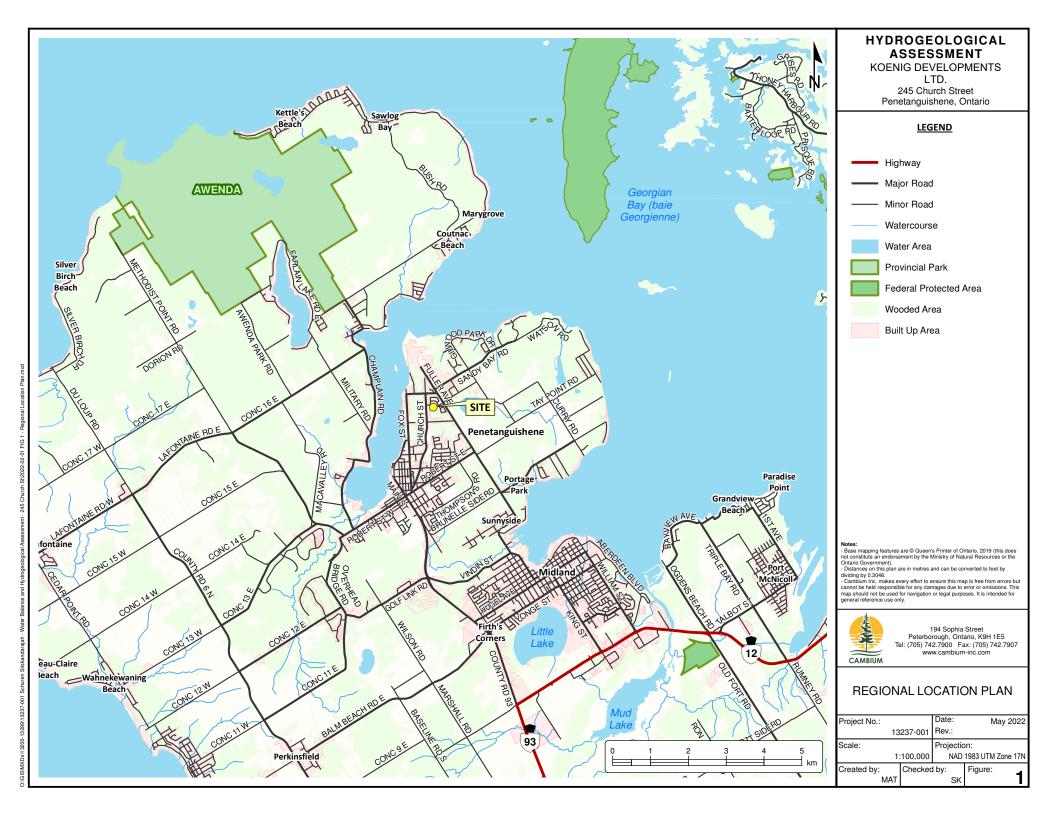
Personal Liability

The client expressly agrees that Cambium employees shall have no personal liability to the client with respect to a claim, whether in contract, tort and/or other cause of action in law. Furthermore, the client agrees that it will bring no proceedings nor take any action in any court of law against Cambium employees in their personal capacity.





Koenig Developments Ltd Cambium Reference: 13237-001 November 15, 2022
Appended Figures



HYDROGEOLOGICAL ASSESSMENT

KOENIG DEVELOPMENTS

245 Church Street Penetanguishene, Ontario

LEGEND

Site (approximate)

Notes:

- Base mapping features are @ Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources or the Ontario Government).

- Distances on this plan are in metres and can be converted to feet by dividing by 0.3048.

- Cambium Inc. makes every effort to ensure this map is free from errors but cannot be held responsible for any damages due to error or omissions. This map should not be used for navigation or legal purposes. It is intended for general reference use only.



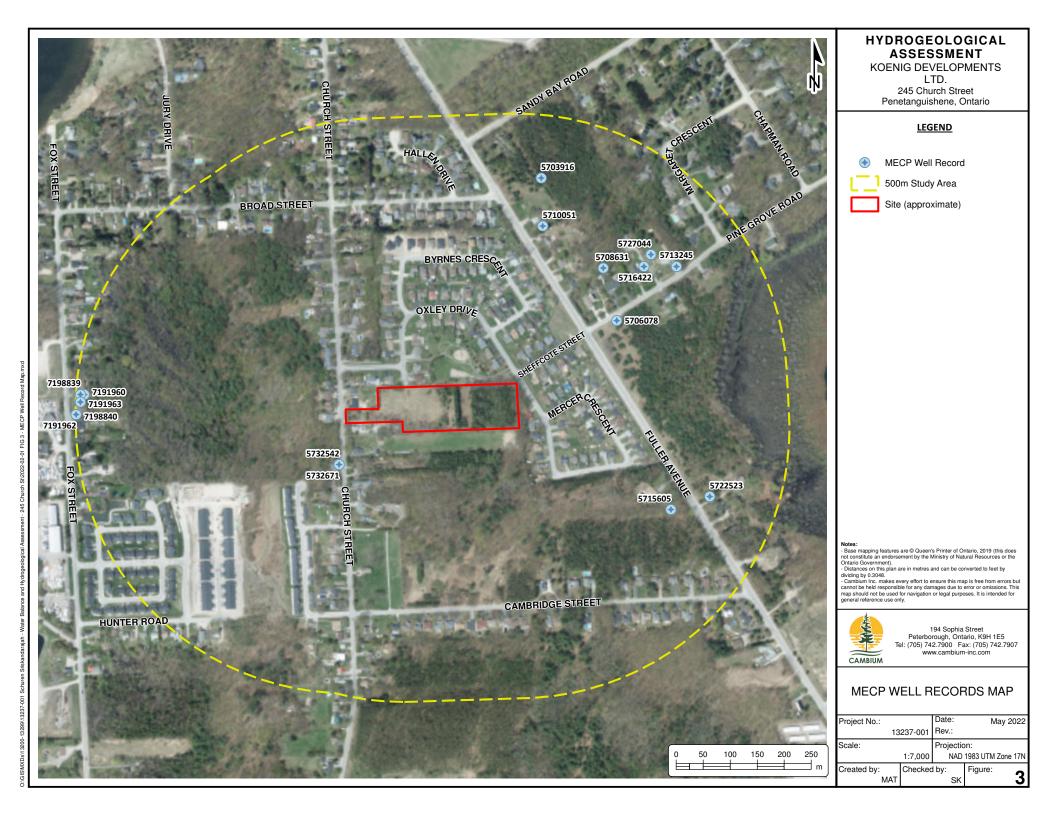
194 Sophia Street Peterborough, Ontario, K9H 1E5 Tel: (705) 742.7900 Fax: (705) 742.7907

SITE LOCATION PLAN

Project No.: May 2022 Rev.: 13237-001

Projection: NAD 1983 UTM Zone 17N 1:1,750

Checked by: Created by: MAT



HYDROGEOLOGICAL ASSESSMENT

KOENIG DEVELOPMENTS

245 Church Street Penetanguishene, Ontario

LEGEND



Borehole



Monitoring Well



Site (approximate)

Notes:

- Base mapping features are @ Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources or the Ontario Government).

- Distances on this plan are in metres and can be converted to feet by dividing by 0.3048.

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194 Sophia Street Peterborough, Ontario, K9H 1E5 Tel: (705) 742.7900 Fax: (705) 742.7907

BOREHOLE LOCATION PLAN

Project No.: May 2022 13237-001 Rev.: Scale: Projection:

NAD 1983 UTM Zone 17N 1:1,750

Checked by: Created by: MAT SK

HYDROGEOLOGICAL ASSESSMENT

KOENIG DEVELOPMENTS LTD.

> 245 Church Street Penetanguishene, Ontario

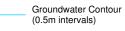
LEGEND



Borehole



Monitoring Well







(218.92) Groundwater Elevation (masl) (May 20, 2022)



Groundwater Flow Direction

Notes:
- Base mapping features are © Queen's Printer of Ontario, 2019 (this does not constitute an endorsement by the Ministry of Natural Resources or the Ontario Government).
- Distances on this plan are in metres and can be converted to feet by dividing by 0.3 must be converted to feet by dividing by 0.3 must be seen to the left of the converted to the conve



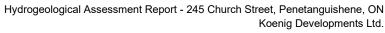
194 Sophia Street Peterborough, Ontario, K9H 1E5 Tel: (705) 742.7900 Fax: (705) 742.7907

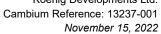
GROUNDWATER **CONFIGURATION MAP**

Project No.: May 2022 13237-001 Rev.: Scale: Projection:

NAD 1983 UTM Zone 17N 1:1,750

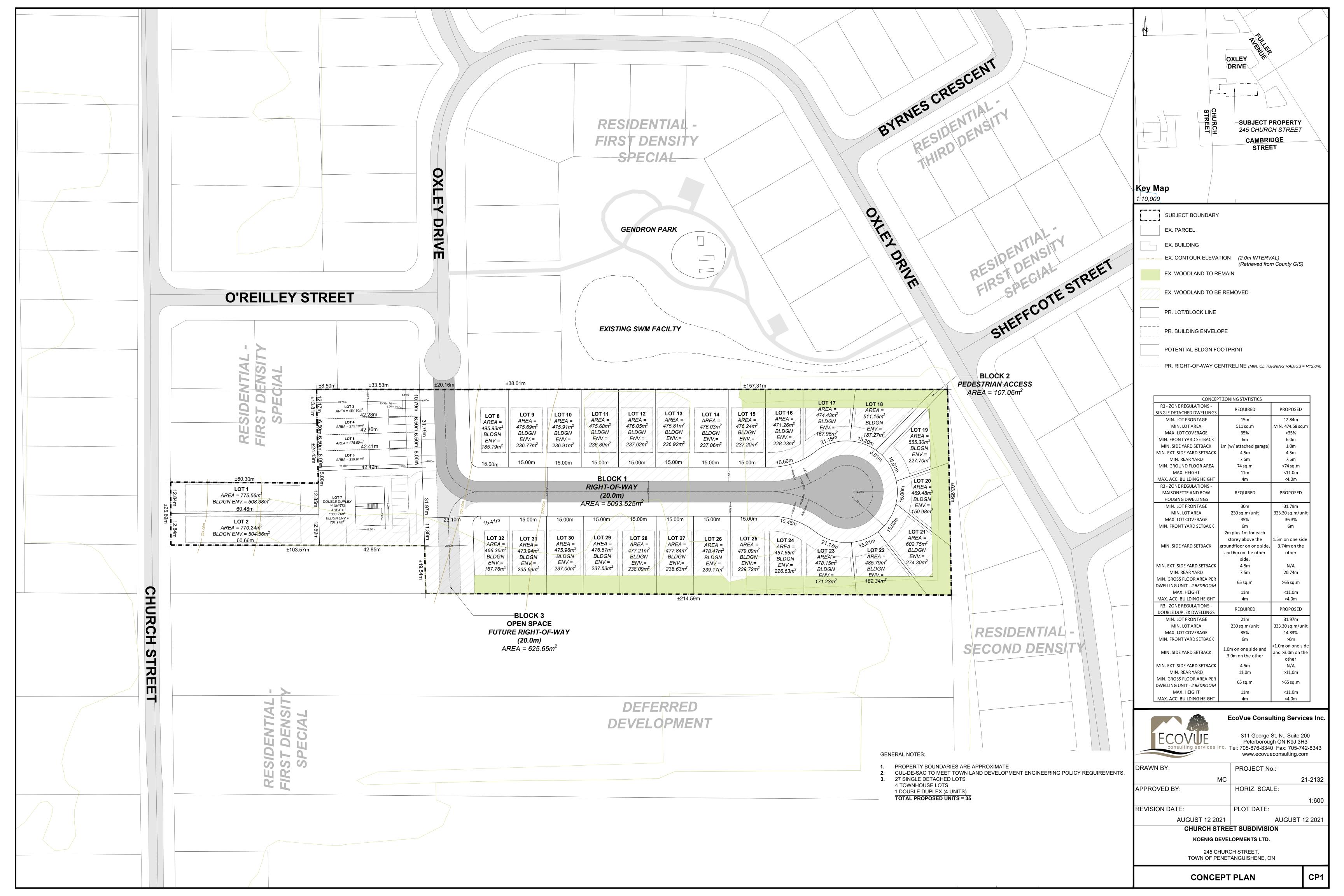
Checked by: Created by: MAT SK

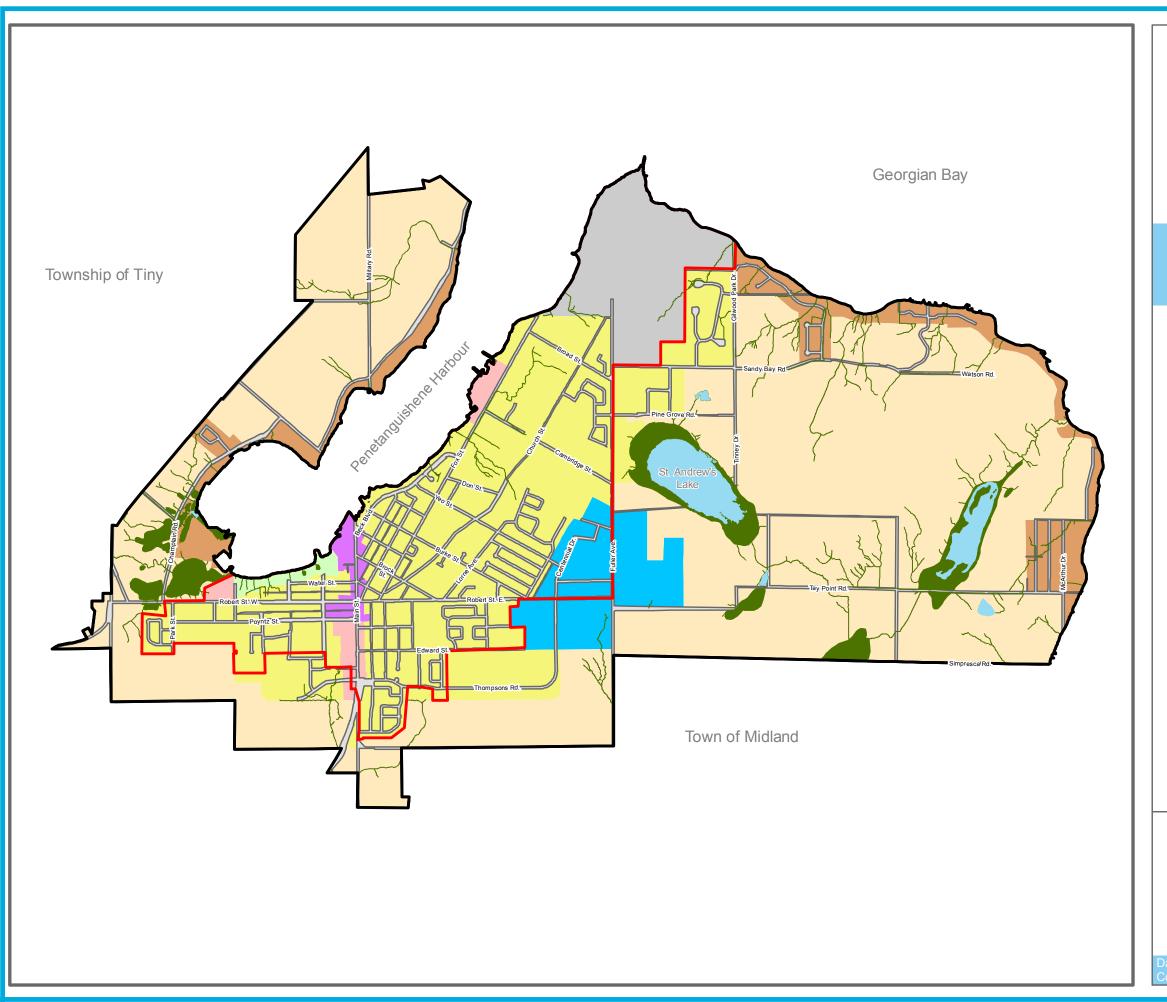






Appendix A
Site Development Plans







OFFICIAL PLAN Schedule A: Land Use Structure

Neighbourhood Area

Downtown and Waterfront Area

Mixed-Use and Commercial Area

Employment Area

Major Open Space Area

Shoreline Area

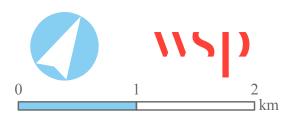
Rural Area

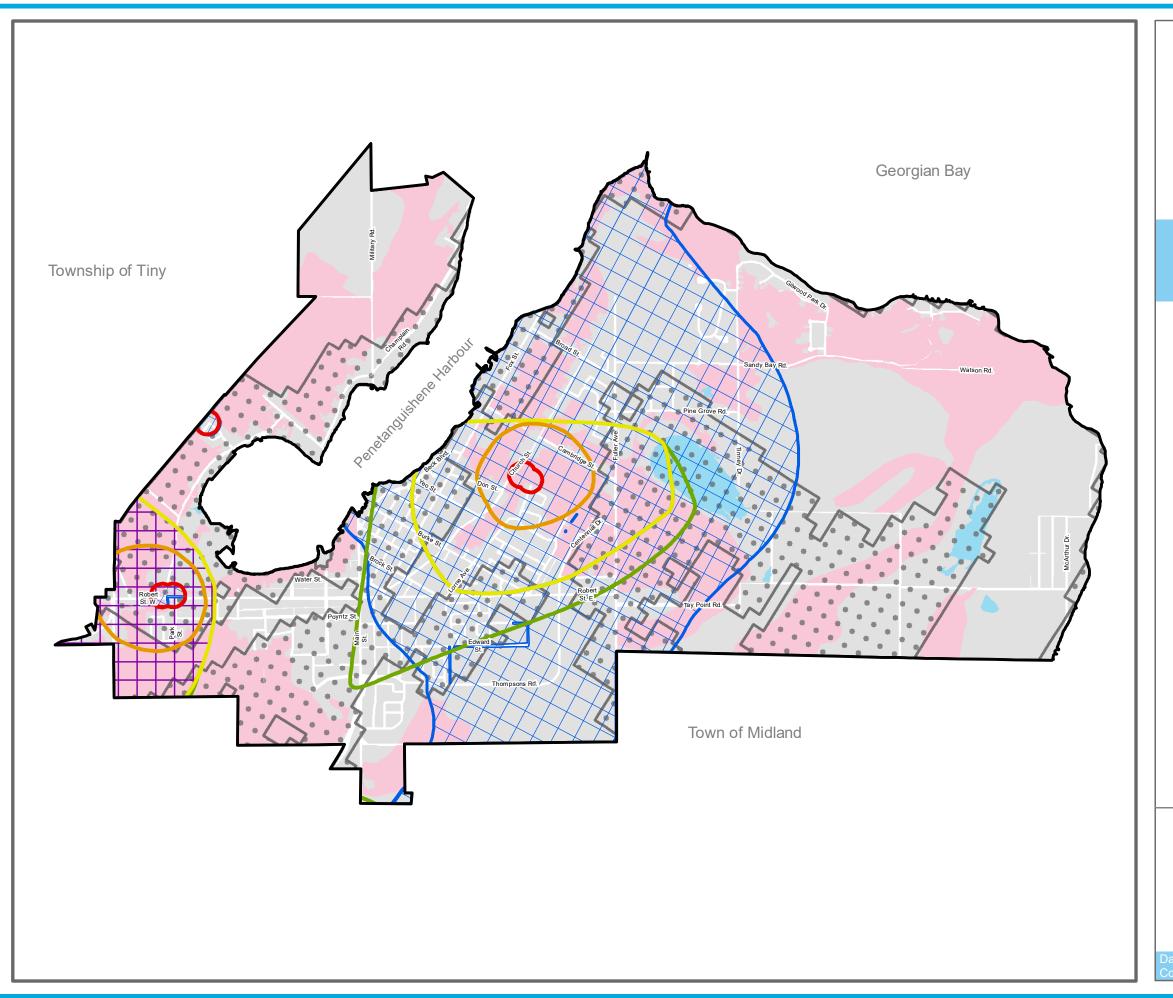
Provincial Institution Area

Environmental Protection Area (EP)

Delineated Built Boundary

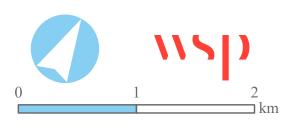
Interpretation Note: This Schedule shall be read and interpreted in conjunction with the Official Plan.

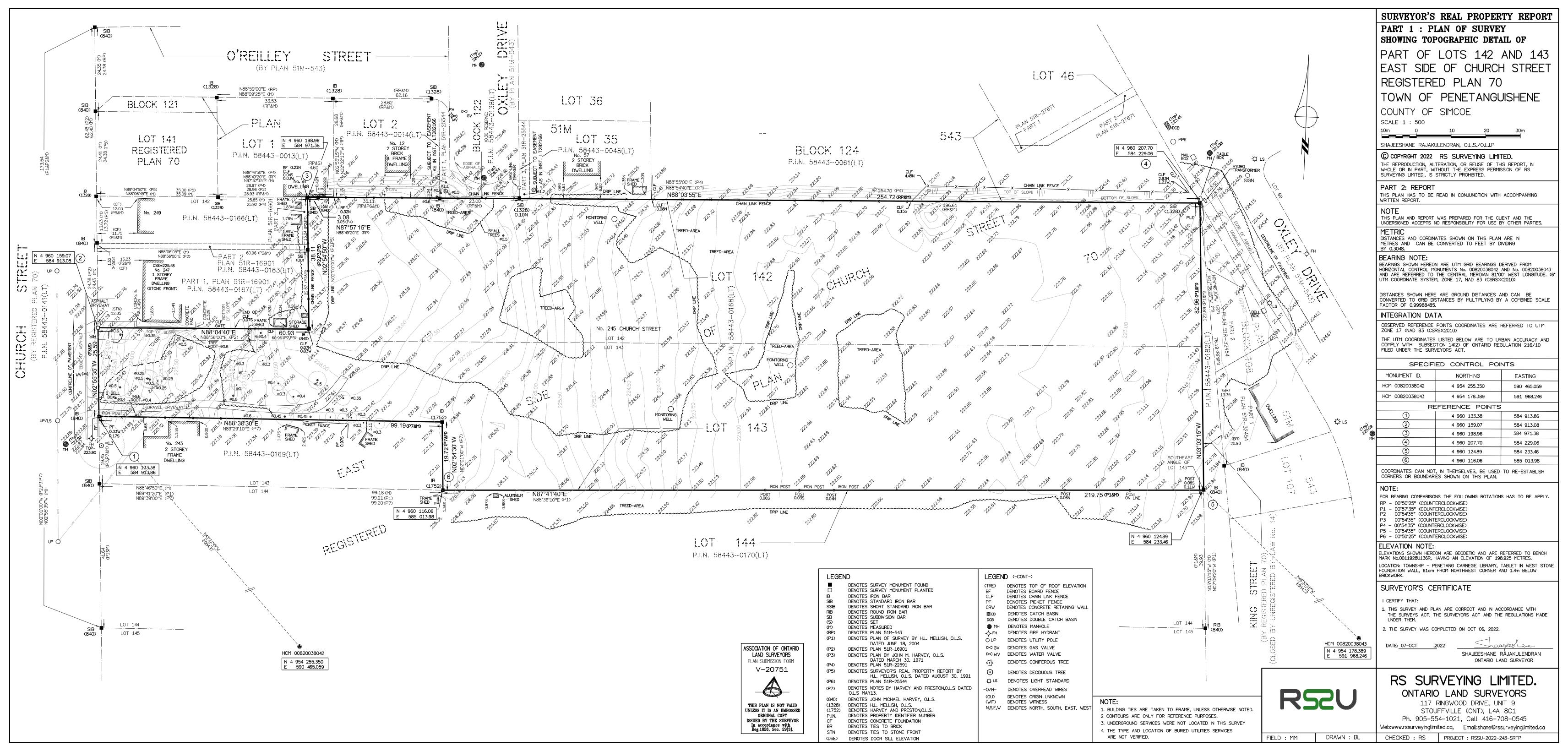






Interpretation Note: This Schedule shall be read and interpreted in conjunction with the Official Plan.





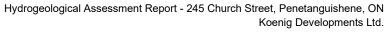
SGRA Map

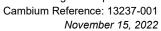




Map Created: 1/12/2022

Map Center: 44.78927 N, -79.92349 W







Appendix B
MECP Well Records

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Brown sand and stone		1	18		
Brown sandy gravel and stones	S	18 68	68 158		
Brown sand and pebbles Brown coarse sand		L 58	169		
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		<u></u>			untested
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Is well on upland, in valley, or on hillside? hillside		road and	lot line. Ind	icate north by	arrow.
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MINISTRY OF THE ENVIRONMENT

310/13W

The Ontario Water Resources Act

WATER WELL RECORD

| 5710051 | MUNICIP. | COLUMN |

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	FINAL 1 M WATER SUPPL	Y 5 ABANDONED, INSUFFICIENT SUPPLY	601	719 SWA
	STATUS 2 OBSERVATION 3 TEST HOLE	7 UNFINISHED		\mathcal{N}
	OF WELL 4 RECHARGE WE	LL '5 □ COMMERCIAL	1 1 1	\mathcal{N}
	WATER 2 STOCK	6 MUNICIPAL 7 PUBLIC SUPPLY		/ /
	USE / 4 INDUSTRIAL	8 COOLING OR AIR CONDITIONING 9 NOT USED	()	
N.	57 CABLE TOOL	6 ☐ BORING		
	METHOD 2 ROTARY (CON	ERSE) 8 🗌 JETTING		
	DRILLING 4 1 ROTARY (AIR) 5 AIR PERCUSSI	i i	DRILLERS REMARKS:	
	NAME OF WELL CONTRACTOR	LICENCE NUMBER	DATA 58 CONTRACTOR 59-62 DATE RECEIV	T50873
	5 ADDRESS Moder N	rilling 4816	SOURCE / 48/6	73
	15 Craishu	rst	# July, 30/7x	M
	ADDRESS ADDRESS NAME OF DRIVER-ON-BOREN SIGNATURE OF CONTRACTOR	LICENCE NUMBER	D REMARKS:	P/5B
	SIGNATURE OF CONTRACTOR	SUBMISSION DATE DAY 5 MO. 08 YR.73	OFFICE 35.79	WI
	Nalsh (In	DAY MO. OO YR.	<u> </u>	100

MINISTRY OF THE ENVIRONMENT The Ontario Water Resources Act L RECORD 5713245 5701 Z 2. CHECK 🗵 CORRECT BOX WHERE APPLICABLE OUNTY OR DISTRICT Tay II P.R.E. Sincoe COMPLETED 04 48-53 OWNER (SURNAME FIRST) 28-47 0 6 yr. **7**6 Box 1023, Barrie, Ont. 21 LOG OF OVERBURDEN AND BEDROCK MATERIALS (SEE INSTRUCTIONS) DEPTH - FEET MOST COMMON MATERIAL GENERAL COLOUR OTHER MATERIALS GENERAL DESCRIPTION 184 0 Sand gravel & Stones 184 200 clay stones 31 32 WATER RECORD 51 **CASING & OPEN HOLE RECORD** 41 SCREEN 0 6000 04 <u> 30</u> DEPTH WATER FOUND AT - FEET WALL THICKNESS' INCHES KIND OF WATER FROM то 1 FRESH 3 SULPHUR 2 SALTY 4 MINERAL stainless sted 1 XSTEEL D 165 2 GALVANIZED 3 CONCRETE 4 OPEN HOLE .188 0 161 1 FRESH 3 SULPHUR 2 SALTY 4 MINERAL 06 0 **PLUGGING & SEALING RECORD** 61 · FEET I [] STEEL 2 [] GALVANIZED 20-Z MATERIAL AND TYPE (CEMENT GROUT, LEAD PACKER, ETC.) 1 FRESH 3 SULPHUR 2 SALTY 4 MINERAL 3 CONCRETE 0165 OPEN HOLE **()200** 1 | FRESH 3 | SULPHUR 2 | SALTY 4 | MINERAL drill cuttings 27-30 1 STEEL 2 GALVANIZED 1 FRESH 3 SULPHUR 2 SALTY 4 MINERAL 30-33 30-33 80 3 CONCRETE MPING TEST METHOD LOCATION OF WELL 2 D BATLER 0004 IN DIAGRAM BELOW SHOW DISTANCES OF WELL FROM ROAD AND LOT LINE. INDICATE NORTH BY ARROW. WATER LEVEL END OF PUMPING 1 D PUMPING 2 RECOVERY 26-2 29-31 32-3 35-37 FEET FEE FEET 1 CLEAR RECOMMENDED RECOMMENDED 43-45 PUMP SETTING SETTING 155 FEET GPM./FT. SPECIFIC CAPACITY FEET RATEO DO 4 Pine Grove RD. WATER SUPPLY OBSERVATION WELL ABANDONED, INSUFFICIENT SUPPLY **FINAL** 6 ABANDONED, POOR QUALITY 7 UNFINISHED STATUS ☐ TEST HOLE OF WELL 4 ☐ RECHARGE WELL DOMESTIC STOCK 5 COMMERCIAL 6 MUNICIPAL WATER ☐ IRRIGATION D PUBLIC SUPPLY USE O ☐ INDUSTRIAL 8 COOLING OR AIR CONDITIONING 9 | NOT USED □ OTHER METHOD 5001 ROTARY (CONVENTIONAL) ROTARY (REVERSE) 7 DIAMOND 3 🗆 8 DETTING OF **DRILLING** s □ AIR PERCUSSION DRILLERS REMARKS CONTRACTOR 659-62 DATE RECEIVED 8 07 7653-68 ONLY ADDRESS ADDRES 4816 DATE OF INSPECT USE NAME EAL STREET ONT. LICENCE NUMBER REMARKS P OFFICE 500 1 Phillip Brown CSS.S8 WΙ Ralph Snider. FORM 7 MOE 07-091

FORM NO. 0506-4-77

The Ontario Water Resources Act WATER WELL RECORD

OUNTY OR DISTRICT	2. CHECK 🗵 CORI	TOWNSHIP, BOROUGH CITY, TOWN VILLAGE			10 1	Y, ETC		22 21 LOT 25-2
		PENETANG.				DATE COMP	_	-19B-
		Simcoe St., Pe		hane	PACIFIC CODE	DAY 0 6	MO1	.0_ YR. 7
	M 10	59.75Q 5	(D, 7,5,0)	چ	22 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
	L	OG OF OVERBURDEN AND BEDROO	K MATERIAL	S (SEE	INSTRUCTIONS)		05.07	H - FEET
NERAL COLOUR	MOST COMMON MATERIAL	OTHER MATERIALS		GENE	RAL DESCRIPTION		FROM	ТО
	sand	gravel					0	56
	sand	stones					56	191
grey	clay						191	193
								-
								-
								-
					MOV	4.0.4000		
					MUV	19 1986		
		total depth: 186 feet						
1) 2056	2811 019			1 1 1 1	1,,,11,1,		1111	
2			لىللىبيا	لل				111
41) WATI	ER RECORD	CASING & OPEN HOLE R			E(S) OF OPENING	31-33 DIAME	TER 34:31 609:96	LENGTH
ATER FOUND AT - FEET	KIND OF WATER	INSIDE DIAM MATERIAL THICKNESS INCHES FRO	EPTH - FEET M TO	8 MA	O14 slot- terial and type tainless .st		DEPTH TO TO	ecker
	FRESH 3 SULPHUR 19 SALTY 4 MINERAL	10-11 1 X STEEL 12 2	13-16	S S	ire wound			180 FEE
	FRESH ³ [] SULPHUR ¹⁹ SALTY ⁴ [] MINERAL	06 4 □ OPEN HOLE 0.188 +	1 0182	61 DEPT	PLUGGIN	IG & SEAI		NENT GROUT
20-23 1 🖂	FRESH 3 [] SULPHUR 24 SALTY 4 [] MINERAL	17-18 STEEL 19 2 GALVANIZED 3 CONCRETE		FRO	M TO 10-13 14-17	MATERIAL AN	D TYPE LEAD	PACKER, ETC
	FRESH 3 SULPHUR 29	4 OPEN HOLE 24-25 1 STEEL 26	27-30		18-21 22-25			
30-33 1 🗆	FRESH 3 [] SULPHUR 34	80 2 GALVANIZED 3 G CONCRETE			26-29 10-33 80			
PUMPING TEST METH	SALTY 4 [] MINERAL OD 10 PUMPING RA	4 ☐ OPEN HOLE			LOCATION	OF WEL	1	
1 K PUMP	2 BAILER	30 30 GPM 02 15-16 00 17-18 HOURS	IN DIA	GRAM BI	ELOW SHOW DISTANC			AND
STATIC LEVEL	PUMPING	1	LOT L		NDICATE NORTH BY	ARROW.		N
122	20	6-28 29-31 32-34 35-37 FEET FEET FEET FEET FEET			`			4
IF FLOWING.	38-41 PUMP INTAK	CE SET AT WATER AT END OF TEST 42				A -		
IF FLOWING. GIVE RATE RECOMMENDED PUNI	P TYPE RECOMMENS	au was we			150x	\ <u>\</u>	-	
SHALLOW		170 FEET RATE 0010 GPM			De Geet	/	LE P	ł
FINAL	t WATER SUPPLY	5 ABANDONED INSUFFICIENT SUPPLY	~	WELL	150 t		12	
STATUS	2 OBSERVATION W	7 UNFINISHED			12 Km		/w	
OF WELL 55	4 RECHARGE WELL	S COMMERCIAL			124			
WATER	2 STOCK 3 RRIGATION	6 MUNICIPAL 7 PUBLIC SUPPLY	İ		_			
USE D	4 🗍 INDUSTRIAL	COOLING OR AIR CONDITIONING NOT USED			` \	/	<u>S</u>	`
METHOD	1 CABLE TOOL 2 ROTARY (CONVI	6 ☐ BORING ENTIONAL) 7 ☐ DIAMOND			1	OBERT !		
OF 4	2 ROTARY (REVER				/ K	U i-		(h
DRILLING	5 AIR PERCUSSIO	N	DRILLERS REMAR					
NAME OF WELL O		ited 4816	DATE OF INSP	, "	4816	DATE RECEIVE	**	63-0
ADDRESS	Drilling Lim		DATE OF INSP	ECTION	INSPECTOR	7 7	117	8
Craigh	rst, Ontario	LICENCE NUMBER	N REPERT	107				
Snider ADDRESS Craight NAME OF DRILLE Ralph S SIGNATURE OF C	Snider.	SUBMISSION DATE	OFFICE	ر مات الم	1 m		CSS.	ES
Ralph S	Snider.	DAY MO YR	0					



MINISTRY OF THE ENVIRONMENT

The Ontario Water Resources Act

WATER WELL RECORD

31013

Simcoe		TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE		CON., BLOCK, TRACT, SURVEY, ETC		LOT 25
		Tav		PRE II	COMPLETED	120 48-53
		Site 14 Comp.	4, Penetar	nguishene DAY	<u>07</u> мо. <u>09</u>	YR. 7
		160200 5	c elevation DI 0750	RC BASIN CODE II	111	lv
2	- 10 12 LC	OG OF OVERBURDEN AND BEDR	OCK MATERIA	LS (SEE INSTRUCTIONS)		
ENERAL COLOUR	WOST COMMON MATERIAL	OTHER MATERIALS		GENERAL DESCRIPTION	DEPTH FROM	· FEET
	sand	boulders			0	36
	sand	stones			36	140
	medium sand				140	191
	sand	silt			191	196
	clay	boulders			196	217
	1imestone	broken			217	225
	limestone				225	233
				<u>a t 0</u> 0		
	,			16,226.		
				~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
10-1	( lack of 1 )	total depth: 182 fee		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	وم ام دا اد م	<u> </u> 
	of 1/ At 1 1 1		1644148		<u> 반속하기 (2) 1</u>	<u>                                      </u>
41 WAT	TER RECORD	51 CASING & OPEN HOLE	RECORD	SIZE(S) OF OPENING 31-33	65 DIAMETER 34-38	75 LENGTH
ATER FOUND AT - FEET	KIND OF WATER	INSIDE WALL THICKNESS THICKNESS	DEPTH - FEET	Z (SLOT NO)  20 slot  MATERIAL AND TYPE	6 INCHES	7.3
, ~ 10·13 1X	FRESH 3 SULPHUR 14 SALTY 4 MINERAL	10-11 XC STEEL 12	13-16	Stainless steel	000 SCREEN P	аскет
15-18 1 [	g FRESH 3 ∏ SULPHUR 19	GALVANIZED CONCRETE  4 D OPEN HOLE	<b>-1</b>  ∴179	61 PLUGGING &	SEALING REC	ORD
	SALTY 4 MINERAL  FRESH 3 SULPHUR 24	17-18 1 ( ) SIEEL 19 2 [ ] GALVANIZED	20-23	DEPTH SET AL FEET MATERI FROM TO MATERI	MADE SALE DATE TO THE SECOND S	ENT GROUT ACKER, ETC
2	SALTY 4 MINERAL  TRESH 3 SULPHUR 29	3 ☐ CONCRETE 4 ☐ OPEN HOLE		10-13 14-17		
2 [	SALTY & MINERAL	24-25 1 C STEEL 26 2 T GALVANIZED	27-30	18-21 22-25 26-29 30-33 80		
2 [	FRESH 3 SULPHUR 34 GC SALTY 4 MINERAL	3 CONCRETE 4 OPEN HOLE	 	26-29 30-33 80		
PUMPING TEST MET	THOO IO PUMPING RATE	E N-14 DUPATION OF PUMPING		LOCATION OF V	N F I I	
	,411	17-18 حريس 16-16 جودر 20 مرم	8			
1 K PUMP	WATER LEVEL 25 END OF WATER L	CC ZU GPM 1 3 HOURS COMMINS	1 IN DIA	AGRAM BELOW SHOW DISTANCES OF INE. INDICATE NORTH BY ARROW.		AND
STATIC LEVEL	WATER LEVEL 25 END OF WATER L PUMPING WATER L 22-24 15 MINUTES	1 D PUMPING 2 DRECOVERY 30 MINUTES 45 MINUTES 60 MINUTES	IN DIA			AND
STATIC LEVEL	WATER LEVEL   25   WATER L   PUMPING	1 ☐ PUMPING 2 ☐ RECOVERY  30 MINUTES 45 MINUTES 60 M.NUTES 28 29-31 32-34 35-3 ET FEET FEET FEET FEE	IN DIA LOT L			AN D
STATIC LEVEL	WATER LEVEL	LEVELS DURING  1  PUMPING  2  RECOVERY  28  29-31  32-34  35-3  ET  FEET  FEET  FEET  SET AT WATER AT END OF TEST  42  FEET  WATER AT END OF TEST  2	IN DIJ LOT L			AND
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU	WATER LEVEL END OF PUMPING  1 22-24 15 MINUTES 26-2 T FEET FEE  38-41 PUMP INTAKE  GPM  IMP TYPE RECOMMENDES PUMP	LEVELS DURING  1  PUMPING  2  RECOVERY  28  29-31  32-34  35-3  ET FEET FEET FEET  SET AT WATER AT END OF TEST 42  FEET FEET CLOUDTY	IN DIA			AND
STATIC LEVEL	WATER LEVEL END OF WATER L PUMPING  1 22-24 IS MINUTES 26-2 T FEET SB-41 PUMP INTAKE  GPM  IMP TYPE PUMP SETTING	LEVELS DURING  1  PUMPING  2  RECOVERY  28  29-31  32-34  35-3  ET FREY FEET FEET  SET AT WATER AT END OF TEST 42  FEET PEET CLOUDY  D 43-45 RECOMMENDED PHYSING  1  PUMPING  2  RECOMMENDED PHYSING  1  PUMPING  2  RECOMMENDED PHYSING  1  PUMPING  2  RECOMMENDED PHYSING  46-41	IN DIA	ine. Indicate north by Arrow.	WELL FROM ROAD	AND
STATIC LEVEL  19-21  125 FEET IF FLOWING, GIVE RATE RECOMMENDED PU SN-53  FINAL	WATER LEVEL END OF WATER L PUMPING  1 22-24 IS MINUTES 26-2 T FEET SB-41 PUMP INTAKE  GPM  IMP TYPE PUMP SETTING	LEVELS DURING  1  PUMPING  2  RECOVERY  28  29-31  32-34  35-3  ET  FEET  FEET  FEET  SET AT  WATER AT END OF TEST  43  FEET  CLEAR 2  CLOUDY  175  FEET RATE	IN DIJ	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET GIVE RATE  RECOMMENDED PU  S0-53	WATER LEVEL END OF WATER L PUMPING  1 22-24 15 MINUTES 26-2 T FEET FEI  38-41 PUMP INTAKE  GPM RECOMMENDES PUMP WATER SUPPLY  54 WATER SUPPLY	LEVELS DURING  1  PUMPING  2  RECOVERY  28  30 MINUTES  45 MINUTES  60 MINUTES  29-31  32-34  35-3  ET  FEET  FEET  FEET  0  43-45  RECOMMENDED  46-41  175  FEET  RATE  69M  ECIFIC CAPACITY  5  ABANDONED, INSUFFICIENT SUPPLY	IN DIA	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET IF FLOWING, GIVE RATE RECOMMENDED PU SHALLOW  50-53  FINAL STATUS OF WELL	WATER LEVEL END OF PUMPING  1 22-24 IS MINUTES 26-2 T FEET FEI  38-41 PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  4 WATER SUPPLY OBSERVATION WEI TEST HOLE RECHARGE WELL  55-56 IN DOMESTIC 2 DOMESTIC 2 STOCK	LEVELS DURING  1  PUMPING  2  RECOVERY  28  30 MINUTES  45 MINUTES  60 MINUTES  29-31  32-34  35-3  ET  FEET  FEET  FEET  FEET  SET AT  WATER AT END OF TEST  42  FEET  CLEAR 2  CLOUDY  0  43-45  RECOMMENDED  46-41  175  FEET  RATE	IN DIJ	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET FLOWING, GIVE RATE  RECOMMENDED PU STATLOW  50-53  FINAL STATUS OF WELL	WATER LEVEL END OF PUMPING  1 22-24 15 MINUTES 26-2  T FEET FEI  38-41 PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  4 GPM./FT. SPE  54 IN WATER SUPPLY 2 GOBSERVATION WEI 3 TEST HOLE 4 RECHARGE WELL  55-56 TOMESTIC 2 STOCK 3 GIRGATION 4 INDUSTRIAL	LEVELS DURING  1  PUMPING 2  RECOVERY  28  29-31  32-34  35-3  ET FEET FEET FEET FEET  D 43-45 PEET RECOMMENDED PARTIES AND PROPERTY AT THE PUBLIC SUPPLY  6  ABANDONED, INSUFFICIENT SUPPLY 1  OWN FINISHED  5  COMMERCIAL 2  OWN FINISHED  5  COMMERCIAL 4  OWN FINISHED	IN DIJ	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU  STATUS OF WELL  SWATER	WATER LEVEL END OF PUMPING  1 22-24 15 MINUTES 26-2  T FEET FEI  WATER L  GPM RECOMMENDES PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  GPM./FT. SPI  WATER SUPPLY 2   OBSERVATION WEI 3   TEST HOLE 4   RECHARGE WELL  S5-56   ODMESTIC 2   STOCK 3   INDUSTRIAL   OTHER	LEVELS DURING  1  PUMPING  2  RECOVERY  28  30 MINUTES  45 MINUTES  29-31  32-34  35-3  ET  FEET  FEET  FEET  D  43-45  RECOMMENDED  46-41  PUMPING  175  FEET  ATE	IN DIJ	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU  STATUS OF WELL  WATER USE  METHOD	WATER LEVEL END OF PUMPING  1 22-24 IS MINUTES 26-2 T FEET SHALL SHALL GPM RECOMMENDES PUMP INTAKE GPM RECOMMENDES PUMP SETTING  GPM /FT SPI  54 IN WATER SUPPLY OBSERVATION WEI TEST HOLE	LEVELS DURING  1  PUMPING 2  RECOVERY  28  29-31  32-34  35-3 ET FEET FEET FEET FEET  D 43-45  RECOMMENDED 46-41  PUMPING 175 FEET ATE GPM ECIFIC CAPACITY  LL 6  ABANDONED, INSUFFICIENT SUPPLY LL 6  ABANDONED, POOR QUALITY 7  UNFINISHED  5  COMMERCIAL 6  MUNICIPAL 7  PUBLIC SUPPLY 8  COOLING OR AIR CONDITIONING 9  NOT USED  6  BORING 110NAL) 7  DIAMOND	IN DIJ	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU  SO-53  FINAL STATUS OF WELL  WATER USE	WATER LEVEL END OF PUMPING  1 22-24 IS MINUTES 26-2 T FEET SH-41 PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  GPM /FT SPE  54 IN WATER SUPPLY OBSERVATION WEI 3 [] TEST HOLE 4 [] DOMESTIC 2 [] STOCK 3 [] IRRIGATION 4 [] INDUSTRIAL [] OTHER  57 I [] CABLE TOOL 2 [] ROTARY (CONVEN 3 [] ROTARY (CONVEN 3 [] ROTARY (CONVEN	LEVELS DURING  1  PUMPING 2  RECOVERY  28  29-31  32-34  35-3 ET FEET FEET FEET FEET  D 43-45  RECOMMENDED 46-41  PUMPING 175 FEET ATE GPM ECIFIC CAPACITY  LL 6  ABANDONED, INSUFFICIENT SUPPLY LL 6  ABANDONED, POOR QUALITY 7  UNFINISHED  5  COMMERCIAL 6  MUNICIPAL 7  PUBLIC SUPPLY 8  COOLING OR AIR CONDITIONING 9  NOT USED  6  BORING 110NAL) 7  DIAMOND	IN DIA	INE. INDICATE NORTH BY ARROW.	WELL FROM ROAD	20
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU  STATUS OF WELL  WATER USE  METHOD OF	WATER LEVEL END OF PUMPING    22-24	LEVELS DURING  1  PUMPING  2  RECOVERY  28  29-31  32-34  35-3  ET FEET FEET FEET FEET  SET AT WATER AT END OF TEST 42  PUMPING  175 FLET PUMPING  ATTE  FEET GFANT  5  ABANDONED, INSUFFICIENT SUPPLY  6  ABANDONED POOR QUALITY  7  UNFINISHED  5  COMMERCIAL  6  MUNICIPAL  7  PUBLIC SUPPLY  6  BORING  9  NOT USED	DRILLERS REMAR	THE INDICATE NORTH BY ARROW.	EE 1 20AD	120 m
STATIC LEVEL  19-21  125 FEET FINAL STATUS OF WELL  WATER USE  METHOD OF DRILLING	WATER LEVEL END OF PUMPING    22-24	LEVELS DURING  1  PUMPING 2  RECOVERY  28  29-31  32-34  35-3  ET FEET FEET FEET FEET  SET AT WATER AT END OF TEST 42  WATER AT END OF TEST 42  PUMPING RATE OF TEST 42  GENERAL GRANDONED, INSUFFICIENT SUPPLY  175 FLET RECOMMENDED POOR QUALITY  TO UNFINISHED  5  COMMERCIAL 6  MUNICIPAL 7  PUBLIC SUPPLY 6  COOLING OR AIR CONDITIONING 9  NOT USED  6  BORING  110NAL) 7  DIAMOND 110NING 9  NOT USED	DRILLERS REMAR	TOUR SEE CONTRACTOR 59-62 DANS	WELL FROM ROAD	1 120 119 (M)
STATIC LEVEL  19-21  125 FEET  FEROWING GIVE RATE  RECOMMENDED PU  STATUS OF WELL  WATER USE  METHOD OF DRILLING	WATER LEVEL END OF PUMPING  1 22-24 15 MINUTES 26-2  T FEET FEI  38-41 PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  4 GPM ATER SUPPLY 2 GOBSERVATION WEI 3 GEST HOLE 4 RECHARGE WELL  55-56 PAGE STOCK 3 GREGATION 4 GOMESTIC 2 GOMESTIC 3 GOMESTIC 3 GOMESTIC 4 GOMESTIC 4 GOMESTIC 57 1 GABLE TOOL 2 GOTARY (CONVEN 3 GOTARY (CONVEN 4 GOTARY (CONVEN 4 GOTARY (CONVEN 5 AIR PERCUSSION  CONTRACTOR  Drilling Limit  CONTRACTOR	LEVELS DURING  2	DRILLERS REMAR  DATA SOURCE  Date of jins	TOUR SEE CONTRACTOR 59-62 DANS	EE 1 20AD	(M)
STATIC LEVEL  19-21  125 FEET  IF FLOWING, GIVE RATE  RECOMMENDED PU  STATUS OF WELL  WATER USE  METHOD OF DRILLING  NAME OF WELL  SOLUTION  NAME OF WELL  ADDRESS	WATER LEVEL END OF PUMPING  1 22-24 15 MINUTES 26-2  T FEET FEI  38-41 PUMP INTAKE  GPM RECOMMENDES PUMP SETTING  4 RECHARGE WELL  55-56 PUMP SETTING  54 RECHARGE WELL  55-56 PUMP SETTING  1 DOMESTIC 2 DOMESTIC 3 DOMESTIC 3 DOMESTIC 3 DOMESTIC 4 ROTARY (CONVEN A ROTARY (CONVEN B ROTARY (CONVEN A ROTARY (CONVEN B ROTARY (CONVEN	LEVELS DURING  1  PUMPING 2  RECOVERY  28  29-31  32-34  35-3  ET FEET FEET FEET FEET  SET AT WATER AT END OF TEST 42  WATER AT END OF TEST 42  PUMPING RATE OF TEST 42  GENERAL GRANDONED, INSUFFICIENT SUPPLY  175 FLET RECOMMENDED POOR QUALITY  TO UNFINISHED  5  COMMERCIAL 6  MUNICIPAL 7  PUBLIC SUPPLY 6  COOLING OR AIR CONDITIONING 9  NOT USED  6  BORING  110NAL) 7  DIAMOND 110NING 9  NOT USED	DRILLERS REMAR	TOUR SEE CONTRACTOR 59-62 DANS	EET 20AD	20

# The Ontario Water Resources Act WATER WELL RECORD

	SPACES PROVIDED RECT BOX WHERE APPLICABLE	5718418	57.012	PR E	02
COUNTY OR DISTRICT	TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE	CON	BLOCK, TRACT, SURVEY ET	PAN 69 0	Constitue
	#1- CTE 14	1- Comp. 5	FAETAND QUE	AY 07 MO 10	
	60250	5 6700 6	BASIN CODE	" ""   ""	iv
10 12	OG OF OVERBURDEN AND BEDRO		INSTRUCTIONS)		
GENERAL COLOUR COMMON MATERIAL	OTHER MATERIALS	GENEF	RAL DESCRIPTION	DEPTH -	FEET TO
BLACK QUERLURDE	Y BOWLDERS			0	14
BLOWN SITT TYPE	Any			/4	42
H. BROWN SAND	(LAYGRED)			42	163
			NOV 18	1986	
			2 0 101		
			161. NA	1	···
(A) Indiana (12)   Long	426 <b>2884</b>   0/6562 <b>8</b> 7473			1 1 1	1 1 1
31   QQ1482513   QQ1	<u> </u>				
WATER RECORD	CASING & OPEN HOLE	RECORD 2 1510	SS OF OPENING ST-	0/000	75 ENGTH 39-40
WATER FOUND KIND OF WATER  10-13 FEET 10-13	INSIDE DIAM MATERIAL THICKNESS INCHES	FROM TO O MAT	TERIAL AND TYPE	DEPTH TO TOP OF SCREEN	41-44 3
0/65 1 FRESH 3 SULPHUR 2/1 SALTY 4 MINERAL	OGO-11 1 X STEEL 12 2 GALVANIZED 11/1/1 1 CONCRETE	13-16	JOHNSON JA	0162	FEET
2 SALTY 4 [] MINERAL	17-18 1 STEEL 15		SET AT FEET MATE		T GROUT
2 SALTY 4 MINERAL	2 GALVANIZED 3 CONCRETE 4 OPEN HOLE	FROM	10-13 14-17	LEADIN	
2 SALTY 4 MINERAL	ZA-ZS 1 STEEL Z6	27-30	18-21 22-25		
30-33 I FRESH 3 SULPHUR 34 2 SALTY 4 MINERAL	3 CONCRETE 4 OPEN HOLE		26-29 30-33 80		
71 Pumping test method 10 Pumping RA	7000 11-14 DURATION OF PUMPING  17-18  17-18  17-18  HOURS  MINS	·	LOCATION OF	WELL	
STATIC WATER LEVEL 25 LEVEL PUMPING WATER	LEVELS DURING  1 PUMPING 2 RECOVERY	IN DIAGRAM BE	LOW SHOW DISTANCES ON IDICATE NORTH BY ARRO		N D
F  /2   //	8-28 29-31 32-34 36-3	7	10 1		
IF FLOWING.  GIVE RATE    D   FEET   D   FEET   FEE	E SET AT WATER AT END OF TEST 42	TO MICHAND.	FINE TAM		
RECOMMENDED PUMP TYPE PUMP	PUMPING	TO MIXAND.	ER AUC.		
SHALLOW DEEP SETTING	/bo FEET RATE OOG GPM		1		
FINAL 2 CBSERVATION W	\$ ☐ ABANDONED, INSUFFICIENT SUPPLY FELL S ☐ ABANDONED, POOR QUALITY	]		N.O.	
STATUS OF WELL   1 TEST HOLE A RECHARGE WELL	7 🗍 UNFINISHED L			Se Constitution of the Con	
SS-SS I DOMESTIC  2 STOCK  WATER  3 IRRIGATION	5 COMMERCIAL 6 MUNICIPAL 7 PUBLIC SUPPLY		3_		7
USE 0 4 INDUSTRIAL	COOLING OR AIR CONDITIONING  The state of th				
METHOD 2 H ROTARY (CONVE	6 ☐ BORING ENTIONAL) 7 ☐ DIAMOND		* /		
OF DRILLING  OF DRILLING  OF DRILLING  OF DRILLING	SE)	001 240	,		
NAME OF WELL CONTRACTOR .	LICENCE NUMBER	DRILLERS REMARKS  DATA SOURCE  58	CONTRACTOR 59-62 DA	<del>16.038</del>	3
ADDRESS PANER SKILL	ING 1652	Source JO DATE OF INSPECTION	INSPECTOR	0	· •
ADDRESS ADDRESS KILL SKILL  NAME OF ORILLER OR BORER  NAME OF ORILLER OR BORER  NAME OF ORILLER OR BORER  SIGNATURE OF CONTRACTOR	LICENCE NUMBER	REMARKS A			
SIGNATURE OF CONTRACTOR	F. Out-	OFFICE	1	CSS.ES	
Loug Houle	DAY 20 MO. 10 YR	¥ [		FORM NO. 0506	



The Ontario Water Resources Act

Ontario of the Enviror			<b>VA</b> 1	ا <b>ا</b>	<b>R I</b>	WELL 23 Mentor	KE.	CO	KD
COUNTY OR DISTRICT	1. PRINT ONLY IN SPA	T BOX WHERE APPLICABLE TOWNSHIP, BOROUGH, CITY.	TOWN, VILLAGE	37	225	CON. BLOCK, TRACT. SI	JRVEY, ETC	_ <u> </u>	01 23 27
		A	/			2 - 1-6A	DATE COMP	LETED "	5 55
			p (-1)	1.11	itio:	ENFLANG	DA1_ <b>G</b>		15
a.	LO(	G OF OVERBURDEN	AND BEDR	OCK MA	TERIAL	.S (SEE INSTRUCTIONS)			
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MATI	ERIALS			GENERAL DESCRIPTION	N	DEPTH FROM	· FEET
	SAND	GRAVEL GRAVE	$(\cdot C)$	Ay				0	35
	SAND	GRAUE	-2				•.	25	60
DXOW4 -	SAND					1754		Q U	110
		,			-				
,						PQ	on 69		
•	•								
31		. Inimial litera							
10 14	R RECORD	51 CASING & C	OPEN HOLE	RECOP		SIZE(S) OF OPENING	31-32 DIAMI	1	75 80 LENGTH 39-40
AI - FEET	KIND OF WATER	INSIDE DIAM MATERIAL INCHES	WALL THICKNESS INCHES	DEPTH - F	TO	MATERIAL AND TYPE		DEPTH TO TOP OF SCREEN	3 FEET
166 : 0 s	GAS II	STEEL 2 GALVANIZED 3 CONCRETE 3 CONCRETE	1.88	0	163	" STAINLESS		163	FEET
2 🗍 S	ALTY 6 □ GAS	4 □ OPEN HOLE 5 □ PLASTIC	149	(	(3 ²⁰⁻²³	DEPTH SET AT - FEET	MATERIAL AN	D TYPE (CEME	ENT GROUT.
20-23   F z	ALTY 6 GAS	1 STEEL 2 GALVANIZED 3 CONCRETE 4 OPEN HOLE 5 PLASTIC	188 1	60 1		FROM TO  10-13 14-17	Stela	The	
2 🗆 5	ALTY 6 GAS	24-25 1 □STEEL 2 □ GALVANIZED 3 □ CONCRETE			27-30	26-29 30-33	go or a	179	
30.33 ,	"" 4 MINERALS	4 □ OPEN HOLE 5 □ PLASTIC							·
71 PUMPING TEST METHOD	BAILER PUMPING RATE	11-14 DURATION OF PI				LOCATIO			
LEVEL	VATER LEVEL 25 WATER LE PUMPING 22-24 15 MINUTES	VELS DURING	PUMPING RECOVERY	_	LOT L	GRAM BELOW SHOW DIST INE INDICATE NORTH	BY ARROW.	FROM ROAD I	AN D
E 120	140 140	140 140	14 / 40 EET / FEE	7			,	1	
IF FLOWING. GIVE RATE  RECOMMENDED PUNP 1	36 41 PUMP INTAKE S	· ·	OF TEST 4.	11		Fuh	IEX ST		
RECOMMENDED PUNP 1	TYPE RECOMMENDED PUMP	43.45 RECOMMENDED PUMPING RATE	20 GP	11			BY ARROW.	1001	
50-53				]					
FINAL STATUS	WATER SUPPLY Description Well Test Hole	\$ ☐ ABANDONED, INSU  6 ☐ ABANDONED POOF  7 ☐ UNFINISHED				ept ST Just	1KM		
OF WELL	4 ☐ RECHARGE WELL	9 DEWATERING			806	ert Stast	1	_	
WATER	STOCK INTRIGATION INDUSTRIAL	MUNICIPAL PUBLIC SUPPLY COOLING OR AIR COND	DITIONING						
USE	OTHER:	9   NO					)		
METHOD "	CABLE TOOL CONVENT CONVENT CONVENT CONVENT	6 ☐ BORING IONAL) 7 ☐ DIAMOND 1 ☐ JETTING			*12			•	
CONSTRUCTION		DIGGING	OTHER	DRILL	ERS REMAR	ks /		173	346
NAME OF WELL CO	NTRACTOR (U) OTER TI	\ l	L CONTRACTOR	<u>۲</u> و د	ATA OURCE	58 CONTRACTOR	59-62 DATE RECEIVE	1 6 198	37
ADDRESS T	UHIER TI	1/2	200		ATE OF INSPE	CTION INSPEC		, , ,,,,	
NAME OF WELL	TECHNICIAN	WELLIC LICE	LL TECHNICIAN		EMARKS		- 519		
SIGNATURE OF TE	ECINICIAN/CONTRACTION	SUBMISSION DATE	1/_ v.8	OFFICE				CSS.ES	· · · · · · · · · · · · · · · · · · ·
LUN		DAY MO	YRLZ	≠					

MINISTRY OF THE ENVIRONMENT COPY

# The Ontario Water Resources Act

# WATER WELL RECORD

	. PRINT ONLY IN SPACES PROVIDED . CHECK 🗵 CORRECT BOX WHERE APPLI	11	5725105	MUNICIP. CON.	ON 02
COUNTY OR DISTRICT		UGH. CITY TOWN, VILLAGE	EON .	BLOCK, TRACT, SURVEY ETC	LOT 25-27 120
OWNER (SURNAME FIRST)	20-47 ADDRESS	<u> </u>	kins field		0MPLETED 48-53 06 NO 06 YR. 89
foldon Cons	EASTING NORTH			ASIN CODE "	111
	LOG OF OVERBL	RDEN AND BEDRO	CK MATERIALS (SEE IN	ISTRUCTIONS)	47
AGENERAL COLOUR I	MOST	HER MATERIALS		L DESCRIPTION	DEPTH - FEET FROM TO
Black Top	Soil				0 1
Red Sa.		1 /		1	1 4
		ulders	Sond	Clan Str	8 76
Crey Cla	Boul	ders grap		9 310	76 105
Red Gras	Jel San	1 0 1/1	rs Hard		105 170
Red Son		1	Clean	· · · · · · · · · · · · · · · · · · ·	170 210
		· · · · · · · · · · · · · · · · · · ·			
31			16 X	X POLE	ا الله
32 10 14 15 41 WATER REC	ORD 51 CASI	NG & OPEN HOLE	SIZE (S		AMETER 34-38 LENGTH 39-40
WATER FOUND KIND OF V	WATER INSIDE MAT	WALL THICKNESS	DEPTH - FEET B 2	O - 18	DEPTH TO TOP 41-44 30 OF SCREEN
1 1 a 2 1 2 11 SALTY 4	SULPHUR  One of the sulphu	L ANIZED / O O	2 190	<u>z</u> z	190 FEET
15-18 1 FRESH 3	SULPHUR SULPHUR GAS  19  4 GONG 4 GOPEN 5 PLAS	TIC 19	61	PLUGGING & SE	CEMENT GROUT
4	SULPHUR 24   1 □STEE 2 □ GALV 3 □ CONC	ANIZED RETE I HOLE	FROM 10	-13 14-17	LEAD PACKER, ETC.
Z SALTY 6	SULPHUR 5 PLAS  MINERALS 24-25  GAS 1 STEE 2 GALV	26 L Anized	27-30	3 Bas	Hole plag
4	SULPHUR 34 10 3 CONT MINERALS 4 COPER GAS 5 PLAS	HOLE	26-	29 30-33 0	
71 PUMP 2 BAILE	1/1/1	2 15-16 17-18 HOURS MINS	L	OCATION OF WI	ELL
STATIC WATER LEVEL END OF PUMPING	WATER LEVELS DURING	PUMPING ,		OW SHOW DISTANCES OF WE	LL FROM ROAD AND
140 151	26-24 29-31	32-34 60 MINUTES 35-37 56 FEET			7
(5)	8-41 PUMP INTAKE SET AT WAT	ER AT END OF TEST 42			
S RECOMMENDED PUMP TYPE	RECOMMENDED 43-45 REC	OMMENDED 46-49 PING			
SHALLOW DEEP	SETTING / / O FEET RAT	E / O GPM	Sand	y Buy Road	
I PINAL -	OBSERVATION WELL . ABANDO	NED. INSUFFICIENT SUPPLY NED POOR QUALITY		3 11 30	
OF WELL	TEST HOLE 7 UNFINIS RECHARGE WELL DEWATER	RING			
2 D	STOCK 5 DOMMERCIAL MUNICIPAL IRRIGATION 7 DUBLIC SUP			ž	
USE		AIR CONDITIONING  9			
METHOD 2	ROTARY (CONVENTIONAL) 7 [	BORING DIAMOND	:		;
CONSTRUCTION • □	ROTARY (AIR) 9 [	JETTING  DRIVING  DIGGING DOTHER	DRILLERS REMARKS		63129
NAME OF WELL CONTRACTOR		WELL CONTRACTOR'S LICENCE NUMBER		ONTRACTOR S9.62 DATE RECE	11 1 0 4000 ·
ADDRESS RH/		1/956	DATE OF INSPECTION	I 44 U JE	JL 1 O 1303
NAME OF WELL TECHNIC	Photos (1)	WELL TECHNICIAN'S	REMARKS	<u> </u>	
SIGNATURE OF TECHNICIAL	N/COMPRACTOR SUBMISS	10547 ON DATE	E S		CSS.ES
	DAY_	7 NO. 0/ YR.0/	0		EORM NO. 0506 (11 / 86) FORM 9



# The Ontario Water Resources Act WATER WELL RECORD

Ontario	1. PRINT ONLY IN : 2. CHECK 🔀 CORR	SPACES PROVIDED	11	572	7044	57012	, ςο,γ, , , ,	02
COUNTY OR DISTRICT	_	TOWNSHIP, BOROUGH, CITY	Y TOWN VILLAGE			COD. BLOCK, TRACT, SURVEY ETC	1.	or 25-27 - M-424
		<u> </u>		c a #	0	DATE	COMPLETED 4	7 yr 90
		ING	SITE 14	CMP 45	A FE	DETANG DAY	i	/ IV
1 2	M 10 12	17 18		26	<u> </u>			<del></del>
	LO	OG OF OVERBURDEN		OCK MAT			DEPTH	FEET
GENERAL COLOUR	COMMON MATERIAL	OTHER MAT	TERIALS			NERAL DESCRIPTION	FROM	то
BROWN	TOPSOIL	ก		-  -			1	23
BROWS	SANO	Boulde	25				73	87
GREY	FINE SANO	7-17-			Fine		87	159
Beown	SAND	GRANE	<u> </u>				159	193
Beown	SAMB	GIORE			, ,,,,			
-						Plon M-42	B	
31	سا لبلبلبل			لسال				
32	14 15	32		43		54 SIZE(S) OF OPENING 31-33	55 DIAMETER 34-38 L	75 80 ENGTH 39-40
WATER FOUND	TER RECORD	INSIDE	OPEN HOLE	DEPTH - FEE	: III	ISLOT NO )	6 INCHES	3 _{FEET}
. , -	FRESH 3 DSULPHUR 14	DIAM MATERIAL INCHES 10-11 1 DESTEEL	INCHES	FROM	13 -16 OO	MATERIAL'AND TYPE  STAINLESS STEEL	DEPTH TO TOP OF SCREEN	41-44 30 11 7 FEET
('1')	6 DGAS  FRESH 3 DSULPHUR	6 /4   2   GALVANIZED 3   GONCRETE 4   GOPEN HOLE 5   DPLASTIC	188	0 1	91 61	PLUGGING & S	SEALING RECO	RD
	SALTY 6 GAS  FRESH 3 SULPHUR 24	17-18 1 DSTEEL	19	•	20-23 01	PTH SET AT - FEET	AL AND TYPE (CEME	NT GROUT CKER. ETC.1
2 [	SALTY 6 GAS	2 □ GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC				10-13 14-17		
2 [	SALTY 6 GAS	1 USTEEL 2 GALVANIZED	6		27-30	10-21 22-25		
	☐ FRESH 3 ☐ SULPHUR 34 34 4 ☐ MINERALS ☐ SALTY 6 ☐ GAS	3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC				26-29 30-33 80		
71 PUMPING TEST ME						LOCATION OF V	VELL	
STATIC	WATER LEVEL 25	S.O GPN HO	DURS MIN	\$	IN DIAGRAM	BELOW SHOW DISTANCES OF INDICATE NORTH BY ARROW.	WELL FROM ROAD A	N D
LEVEL 19-20	PUMPING	30 MINUTES 45 MINUTES	RECOVERY 5- 60 MINUTES 2-34 35-3	- 7				
		EET FEET	FEET FEE	т		- 600'		
IF FLOWING. GIVE RATE  RECOMMENDED PI	GPM	1 .	R 2 ☐ CLOUDY			PINE GROVE R	Φ.	
RECOMMENDED PO	PHMP	A3-45 RECOMMENDED PUMPING RATE	8.0 60	1	<b>-</b> 70			
50-53		-06		]	<u>ن</u> ر	0-0-T S-T		
FINAL	1 WATER SUPPLY 2 OBSERVATION WE	S ABANDONED, INST			FOUR PROPERTY OF THE PROPERTY	ROBERT ST		
STATUS OF WELL	3 TEST HOLE 4 RECHARGE WELL	7 UNFINISHED  DEWATERING			·			
j	55-56 1 DOMESTIC 2 STOCK	5 COMMERCIAL 6 MUNICIPAL			A C W			
WATER USE	3   IRRIGATION 4   INDUSTRIAL	7 PUBLIC SUPPLY  8 COOLING OR AIR CON						
	0 OTHER	9 NO	J: USED	-				
METHOD OF	1 CABLE TOOL		o .				C	5 <b>E</b> 20
CONSTRUCT		9   DRIVING	. □ OTHER	DRILLER	RS REMARKS		∵o ———	5529
NAME OF WELL	L CONTRACTOR	, MFI	L CONTRACTOR	II > Isome		265 2 DATE R	ECEIVED O 400	63-64 60
C ADDRESS	WEL DRILL	NA	1652.	O DATE	OF INSPECTION	INSPECTOR	AUG 28 199	U
NAME OF WE		OWATER ON	T	S O REM	APKS		**************************************	
	im HowEL		11057	OFFICE				
SIGNATURE O	F TECHNICIAN/CONTRACTOR	1	07 YR.9				CSS.E	<u>S</u>
<u>, ~</u>							FORM NO. 0506 (	11/86) FORM 9



MINISTRY OF THE ENVIRONMENT COPY

# The Ontario Water Resources Act WATER WELL RECORD

Untario  1. PRINT ONLY IN	SPACES PROVIDED	11	5728101		<u> </u>
COUNTY OR DISTRICT	OWNSHIP BOROUGH, CITY,	TOWN, VILLAGE	<b>6</b>	BLOCK TRACT, SURVEY, ETC	120
	ay	- 100 - 200 - 200	0 11 011	DATE	COMPLETED 48-53
	ng R	R#1	RIKINS FIRE	BASIN CODE II	06 no 66 yr 91
1 2 M 10 12	17 18	1 49	42TP !	31	
	OG OF OVERBURDEN	AND BEDRO	CK MATERIALS (SEE )	NSTRUCTIONS)	DEPTH - FEET
GENERAL COLOUR COMMON MATERIAL	OTHER MATE	RIALS	GENER	AL DESCRIPTION	FROM TO
Black T Soic					0 2
Red Sold					2 4
Red grovel	Stone Boulde	· S			4 105
grey Cloy	Boulde	J \$	2+1	grave (	705 170
Red Sand			hard	, Clean	170 210
		·			
;					
31	<u> </u>	1,1,1,1		1,,,11,1,1,1	
32					
41 WATER RECORD	51 CASING & C	PEN HOLE R	RECORD SIZE (SLO	T NO I	DIAMETER 34-38 LENGTH 39-40
WATER FOUND KIND OF WATER	INSIDE MATERIAL	WALL D TH:CKNESS INCHES FRU	1 6	ERIAL AND TYPE	DEPTH TO TOP 0F SCREEN 41-44 30
203 1 GARESH 3 DSULPHUR 14	10-11 1 STEEL 12		13-16	SS	190 FEET
15-18 1   FRESH 3   SULPHUR 19	2 GALVANIZED 3 CONCRETE 4 COPEN HOLE 5 PLASTIC	264 + 2	,		SEALING RECORD
20-23 1   FRESH 3   SULPHUR 24	17-18 1 STEEL 2 GALVANIZED		20-23 DEPTH FROM	SET AT - FEET MATERIA	AL AND TYPE (CEMENT GROUT LEAD PACKER, ETC.)
2 SALTY 4 DMINERALS  25-28 1 FRESH 3 DSULPHUR 29 4 DMINERALS	3 CONCRETE 4 OPEN HOLE 5 PLASTIC		06		ment
2 U SALIT 6 DGAS	24-25 1 STEEL 26 1 STEEL 26 2 GALVANIZED 3 CONCRETE			8-21 22-25 Bend	tod-le
1   FRESH 4   MINERALS 2   SALTY 6   GAS	4 OPEN HOLE 5 PLASTIC			Net	de plue
71 PUMPING TEST METHOD 10 PUMPING RA	50 GPM 2 15-14	6 17-18	1	OCATION OF W	VELL
CYATIC WATER LEVEL 25	LEVELS DURING	PUMPING RECOVERY		OW SHOW DISTANCES OF V DICATE NORTH BY ARROW.	WELL FROM ROAD AND
() 19-21 22-24 15 MINUTES	30 MINUTES 45 MINUTES	60 MINUTES			ブ
	20 148-31 148-6EET WATER AT END C	ET / SFEET			
IF FEET TO FEE	, , CEI	2 CLOUDY	•		
RECOMMENDED PUMP TYPE  SHALLOW DEEP  RECOMMENDED  PUMP  SETTING	43-45 RECOMMENDED PUMPING RATE	70 GPM	7		
50-53			= Soud.	, los Pl	
FINAL 1 WATER SUPPLY 2 OBSERVATION W	S ABANDONED, INSUF		5 3.	<del>1</del>	lbn.
STATUS  OF WELL  TEST HOLE  RECHARGE WELL	, UNFINISHED		A Am	ite.	<b>9</b>
55-56 1 DOMESTIC 2 STOCK	S G AUNICIPAL		-		
WATER  J IRRIGATION  USE  4   INDUSTRIAL	7 DEPUBLIC SUPPLY  COOLING OR AIR CONDI				
57 O	9 🗆 `NOT	USED			j
METHOD 2 ROTARY (CONVE					
OF CONSTRUCTION  Great Rotary (Revers  Description of the procession of the processi	9 DRIVING	OTHER	DRILLERS REMARKS		103639
NAME OF WELL CONTRACTOR	WELL	CONTRACTOR'S	DATA SE	CONTRACTOR 59-62 DATE R	ECEIVED 63-68 80
	Ing (TD LICE)	456	SOURCE DATE OF INSPECTION	1456 J	UN 1 7 1991
RPHI OR	20 STATIL		JSE		
ADDRESS  ADDRESS  NAME OF WELL TECHNICIAN  DAUD  SIGNATURE OF TECHNICIAN/COMPACTOR	S N	TECHNICIAN'S			
SIGNATURE OF TECHNICIAN CONTRACTOR	SUBMISSION DATE  DAY 66 Mg.	36 9/	OFFICE		CSS.ES
LI A COM	MO.	YR			FORM NO. 0506 (11/86) FORM 9

### The Ontario Water Resources Act WATER WELL RECORD

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Mark correct box with a checkmark, where applicable.

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Municipality	Con.						
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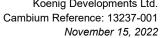
County	or District	•				Borough/City/	Town/Village	und	1 ONT	Con blo	ck tract survey	, etc. Lot	25-27
					PE A Address		yn g	4154	PENE	1029	Date	9 10	v 46
					1406	Northing	NIB	RC Eleva	ation RC	Basin Cod	completed e	day mor	iv year
21		,	M 10	12		18	24	25 26		31			47
					VERBURDEN		ROCK MA	TERIALS (		al description		Dep	th feet
Genera	al colour		common materia	<u> </u>	Oth	er materials			401101			From	<u></u>
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31	1-1-			<u> </u>					<u>                                     </u>				
41	WA	TER RECO	RD	51	CASING &				(Clot N	of opening	31-33 Diameter	34-38 Lengt	75 80 h 39-40
Water f		Kind of v		Inside diam inches	Material	Wall thickness inches	Deptr From	- feet To	EE	10	0 2	Depth at top of	of screen 30
	1 1 1	3 - 1 4	☐ Sulphur 14 ☐ Minerals ☐ Gas		Steel 12 Galvanized	;		13 - 16	SCI	al and type  A 51	c	193	7 feet
	1 1 1	☐ Fresh ^{3 ⊆}	Sulphur 19 Minerals	64	Concrete Open hole Plastic		0	203	61	PI UGG	ING & SEALI	NG RECOR	D D
		C Front 1	Gas Sulphur 24	. 2	☐ Steel 19 ☐ Galvanized			20-23	Depth set	Annular sp		☐ Abandonm	
		Salty 6	Minerals Gas Sulphur 29	2"	☐ Concrete ☐ Open hole ☑ Plastic		+2	193	From	То	laterial and type (C		
		⊓ Saltv 4 ĺ	☐ Minerals ☐ Gas	24 25 1	Steel 26 Galvanized			27-30	Ø-13	190	BENS	Dlu	7
	1 1 1	D 0-16. 4 (	Sulphur 34 60 Minerals	3	☐ Concrete ☐ Open hole ☐ Plastic				100	203	HOLE NO3.	8RAV	re L
	mping test		Gas Pumping rate	11-14	Duration of pumpi	ing	\ 1						
	Pump 2	☐ Bailer	25	GPM	Hours	Mins	-	In diagran	-	OCATION w distance:	or well from re	oad and lot li	ine.
		Water level end of pumpin	<u> </u>	during		Recovery 60 minutes	$\ $	Indicate n	orth by arro	w.			
PUMPING TEST	73		26-28	29-31 feet	32: 34 . feet	35-37 <b>feet</b>	·		012	682			9
NIC III	feet   flowing give		Pump intake set	at	Water at end of te	est 42	11		<b>^</b>	9			3
Re	commende	GPN d pump type	Recommended pump setting	feet 43-45	Clear Recommended pump rate	☐ Cloudy	1		,	9			do
1 1 1	Shallow	☐ Deep	parity setting	feet	panip rate	GPM			<b>%</b>	7			7
	LSTATI	JS OF WEL	L 54			hod	<u> </u>		\$	Ž			1,3
1 2 3		ation well	6 ☐ Abandoned, 7 ☐ Abandoned	poor quality	ıpply 9 ☐ Unfinis ıa ☐ Replac	cement well			<u> </u>				
4	Recharg		8 Dewatering					YEO	STRE	KN78			
1 ,	ER USE	tic	55.56 5 Commercial		₉ ☐ Notus					O.E.			Kon
; 3	Stock Irrigation		s ☐ Municipal □ Public supp □ Cooling & a		·-		11				o C+		- 1/4.4
			CTION 57				11		STRE				1
METH	Cable t	CONSTRU  ool (conventional)	6 ☐ Boring	ion	9 ☐ Driving		$\parallel$		<i></i>	2416	hene 1		
3	Rotary Rotary	(reverse)	/ Diamond				$\parallel f$	ENE	מאות ך	יכוטן	1	7679	1
<u> </u>					I Mail Control	tor's Linence N-		ata				eceived	63-68 80
Name	DY /	ntractor INNER	QUELL DR	Ilino E		tor's Licence No		urce 	58 Contract	5 14	NO		996
Addre	CH	مده زار	ent SI	(/.,)	Ropeir	s out	USEO	ate of inspection	n	Inspector		· ·	
yarne	of Well Tec	W/ WC	N 5/	LN)	AACH (CCIRIIC)	all's Licepce III		emarks	· · · · ·			*.*	
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# The Ontario Water Resources Act WATER WELL RECORD

Ontario	1. PRINT ONLY IN	SPACES PROVIDED ECT BOX WHERE APPLICABLE	11	57326	71	5,7,6,0,6	5		
COUNTY OR DISTRICT	Z. CHECK ZS CORR	TOWNSHIP, BOROUGH, CIT	Y. TOWN. VILLAGE	,	CON B	LOCK, TRACT, SURV	EÝ, ETC		22 23 74 LOT 25-27
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41 WATER	RECORD	51 CASING &	OPEN HOLE I	RECORD		OF OPENING	31-33 DIAMET	ER 34-38	75 80 LENGTH 39-40
AI - FEET	ND OF WATER	INSIDE DIAM MATERIAL INCHES	THICKNESS	DEPTH - FEET	MATERI OS	AL AND TYPE	1	2 INCHES	39 FEET
250 10-13 1 = FRE		10-11 1 TOTEEL 1.	- inches	13-16	Solo	inter S	lex!	OF SCREEN	1/2 FEET
15-18 1 G FRE	SH 3 DSULPHUR 19	2 GALVANIZED 3 CONCRETE 4 OPEN HOLE 5 DPLASTIC	*3/3 A	0 060	61	PLUGGIN	G & SEAL	ING RECO	ORD
20:23 1 pre	SH 3 SULPHUR 24	5 UPLASTIC	•	2 250	DEPTH SE	TAT - FEET	MATERIAL AND		ENT GROUT ACKER, EFC )
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2 - SAL	TY 6 GAS	24-25 1 STEEL 20 GALVANIZED		27-30	18-21	22-25	PENSON	ile S	Tuppy
30-33 1	4 MINERALS	3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC			26-29	30-33			
71 PUMPING TEST METHOD	10 PUMPING RATE	11-14 DURATION OF P	i		LO	CATION	F WEL		
I SIRILE   ,	ER LEVEL 25	/// GPMHO	PUMPING			SHOW DISTANCE		ROM ROAD	AND
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T FLOWING. GIVE RATE  RECOMMENDED PUMP TYP	38-21 PUMP INTAKE S		OF TEST ZZ	CP.	284				F
RECOMMENDED PUMP TYP	PUMP		46-45		Ø				•
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NAME OF WELL	WELL DRI	Hing 34	06	O DATE OF INSPEC		NSPECTOR	rcb /	/ 133/	
A RR # G	RAND U	alley C	L TECHNICIAN'S	S REMARKS	at days				
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				11 - 21 - 1					







Appendix	C
Borehole Log	ζS



Log of Borehole:

BH101-21 Page 1 of 1

T: 866-217-7900

www.cambium-inc.com

Client:Koenig Developments Ltd.Project Name:245 Church Street, Penetanguishene, ONProject No.:13237-001Contractor:Walker DrillingMethod:Hollow Stem AugerDate Completed:July 21, 2021

Location: 245 Church Street, Penetanguishene, ON UTM: 17T, 4960179 m N, 584981 m E Elevation: 228.16 mASL

	;	SUBSU	RFACE PROFILE				SAM	PLE		
Elevation	(m) Depth	Lithology	Description	Number	Type	% Recovery	SPT (N) / DCPT	% Woistrue % NO SPT (N) / (N) 20 30 40 25 50 75 10 20 30 40	Well Installation	Remarks
228 -	0 		TOPSOIL: Black sand, some silt, with organics, loose, moist [TOPSOIL] SAND: Brown sand, some silt, trace	1A 1B	SS	60	6			
227 -	† † †−1 †-		clay trace gravel, loose, moist	2	SS	90	5			
226 -	- - - - 2		SILTY SAND: Grey silty sand, trace gravel, compact, moist	3	SS	80	20			GSA SS3: 7% Gravel 68% Sand 25% Silt and Clay
225 -	   3		-trace cobbles, very dense	4	SS	70	50/ 280 mm			
224 -				5	SS	80	230 mm			
	- - - - - -5			6	SS	10	50/ 150 mm			
223 -										
222 -	- - - - -		Borehole terminated at 6.6 mbgs	7	SS	50	50/ 125 mm			
221 -	<del></del>		due to target depth achieved.							Borehole open and dry upon completion of drilling
	_									•

BW



Log of Borehole:

BH102-21

Page 1 of 1

T: 866-217-7900 www.cambium-inc.com

Project Name: Project No.: Client: Koenig Developments Ltd. 245 Church Street, Penetanguishene, ON 13237-001 Contractor: Walker Drilling Method: Hollow Stem Auger Date Completed: July 21, 2021

Location: 245 Church Street, Penetanguishene, ON UTM: 17T, 4960189 m No, 585057 m East Elevation: 224.67 mASL

	;	SUBSU	RFACE PROFILE				SAM	IPLE			
Elevation	(m) Depth	Lithology	Description	Number	Type	% Recovery	SPT (N) / DCPT	% Moisture	/ (N) LdS	Well Installation	Remarks
	- <b>O</b>	\( \frac{\lambda}{\lambda} \)	TOPSOIL: Black sand, some silt, with organics, loose, moist [TOPSOIL] SAND: Brown sand, some silt, trace	1A 1B	SS	90	6			Monument Cap	Top of Pipe (TOP) elevation: 225.46 mASL. Groundwater measured at 5.95
224 -	-[ - - 1 -		clay, trace gravel, loose, moist -less silt content	2	SS	80	7			Bentonite	mbgs (218.72 m Rel. El.) on July 6, 2022
223 -	- - - - - - -			3	SS	70	6			Plug PVC Standpipe	GSA SS2: 1% Gravel 80% Sand 15% Silt 4% Clay
222 -	2 			4	SS	70	9			XXXXXX	
	 3 		-compact	5	SS	70	21			000000000000000000000000000000000000000	
221 -										Sand Pack PVC Screen	
220 -			SILTY SAND: Grey silty sand, some gravel, trace clay, very dense, moist	6	SS	70	50		\	PVC Screen	GSA SS6: 11% Gravel 62% Sand 24% Silt
219 -	- - - - -									Can	3% Clay
	6 			7	SS	0	50/ 100 mm			Cap	
218 -			Borehole terminated at 6.6 mbgs due to target depth achieved.								
	1										

BW

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Log of Borehole:

BH103-21

Page 1 of 1

T: 866-217-7900

www.cambium-inc.com

Project Name: Project No.: Client: Koenig Developments Ltd. 245 Church Street, Penetanguishene, ON 13237-001 Contractor: Walker Drilling Method: Hollow Stem Auger Date Completed: July 21, 2021

Location: 245 Church Street, Penetanguishene, ON UTM: 17T, 4960146 m N, 585079 m E Elevation: 223.86 mASL

		SUBSU	RFACE PROFILE				SAM	IPLE			
Elevation	(m) Depth	Lithology	Description	Number	Type	% Recovery	SPT (N) / DCPT	25 75 Woistrue	/ (N) LdS 030 40	Well Installation	Remarks
	<b>0</b>	\( \frac{1}{2} \)	TOPSOIL: Black sand, some silt, with organics, loose, moist [TOPSOIL]  SAND and SILT: Brown sand and silt,	1A / 1B	SS	60	3			Monument Cap	Top of Pipe (TOP) elevation: 224.70 mASL. Groundwater measured at 5.92
223 -	- - - 1		trace gravel, loose, moist -trace cobbles	2	SS	100	3				mbgs (217.94 m Rel. El.) on July 6, 2022
			-grey, no cobbles							Bentonite Plug PVC Standpipe	GSA SS2: 3% Gravel 62% Sand
222 -			B. 27, 110 00001E3	3	SS	50	7				35% Silt and Clay
221 -			-compact	4	SS	60	21			3000000000	
	3 			5	SS	0	20				
220 -	<b>4</b> <b>4</b>									Sand Pack PVC Screen	
219 -	_ _ _ _ 5		-dense	6	SS	90	39			PVC Screen	
	- - - -									Can	
218 -	6 6		-very dense, wet	7	SS	90	50/ 280 mm			Cap	
217 -	 - 7		Borehole terminated at 6.6 mbgs due to target depth achieved.								
	-[ -[										

BW

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Log of Borehole:

BH104-21 Page 1 of 1

T: 866-217-7900

www.cambium-inc.com

Client:Koenig Developments Ltd.Project Name:245 Church Street, Penetanguishene, ONProject No.:13237-001Contractor:Walker DrillingMethod:Hollow Stem AugerDate Completed:July 21, 2021

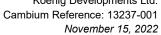
Location: 245 Church Street, Penetanguishene, ON UTM: 17T, 4960145 m N, 585117 m E Elevation: 222.65 mASL

	ļ	SUBSU	RFACE PROFILE				SAM	IPLE			
Elevation	(m) Depth	Lithology	Description	Number	Туре	% Recovery	SPT (N) / DCPT	% Woistrue	/ (N) Ld OO 10 20 30 40	Well Installation	Remarks
222 -	- <b>O</b>	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	TOPSOIL: Black sand, some silt, with organics, loose, moist [TOPSOIL]  SAND: Brown sand, trace gravel, trace silt, loose, moist	1A 1B	SS	90	4			Monument Cap	Top of Pipe (TOP) elevation: 223.49 mASL. Groundwater measured at 6.14
	 _ <b>1</b> 		-trace cobbles, wet	2	SS	80	8			Bentonite Plug	mbgs (216.51 m Rel. El.) on July 6, 2022
221 -	    2			3	SS	60	6			PVC Standpipe	
220 -	-    		-trace clay, compact	4	SS	70	16			30000000000000000000000000000000000000	GSA SS4: 4% Gravel 87% Sand 9% Silt and Clay
219 -	_ <del> </del> _3   			5	SS	80	21				
213	- <b>-4</b> <b>-4</b> 									Sand Pack PVC Screen	
218 -	  5		-very dense	6	SS	0	50/ 205 mm		\	Screen	
217 -	1 - - - -									Can	
	_ <b>-6</b>  		-saturated	7	SS	60	50/ 180 mm			Cap	
216 -	  <b>7</b>  		Borehole terminated at 6.6 mbgs due to target depth achieved.								
	L			<u> </u>		<u> </u>	<u> </u>			<u>l</u>	<u> </u>

BW

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	Αp	pend	İX	D
Grain S	Size	Anal	ys	is





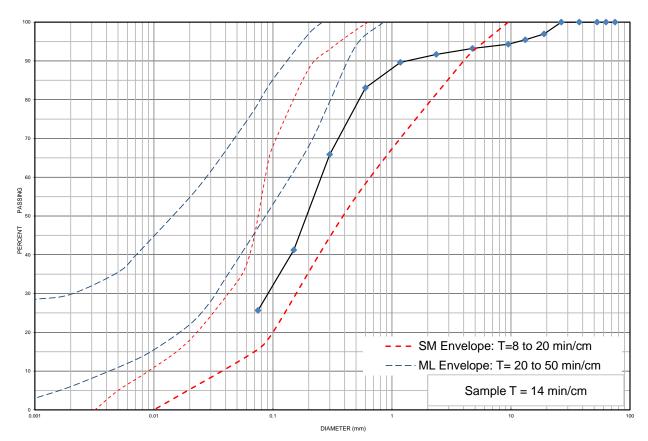
Project Number: 13237-001 Client: Koenig Developments Ltd.

Project Name: Water Balance and Hydrogeological Assessment - 245 Church St

Sample Date: July 21, 2021 Sampled By: Ben White - Cambium Inc.

**Location:** BH 101-21 SS 3 **Depth:** 1.5 m to 2 m **Lab Sample No:** S-21-0882

UNIFII	ED SOIL CLASSIF	ICATION SYSTE	М		
OLAMA OUT ( O OTS )	SAND (<4.	GRAVE	L (>4.75 mm)		
CLAY & SILT (<0.075 mm)	FINE	MEDIUM	COARSE	FINE	COARSE



	MIT SOIL CLASSIFICATION SYSTEM										
CLAY	SILT	FINE	MEDIUM	COARSE	FINE	MEDIUM	COARSE	DOLU DEDC			
CLAT	SILI		SAND			GRAVEL		BOULDERS			

Borehole No.	Sample No.		Depth	Gravel		Sand	Si	ilt	Clay	Moisture
BH 101-21	SS 3		1.5 m to 2 m	7		68				9.5
	Description		Classification	D ₆₀		D ₃₀		D ₁₀	Cu	C _c
Silty Sand trace Gravel		SM	0.255		0.090		-	-	-	

Additional information availabe upon request





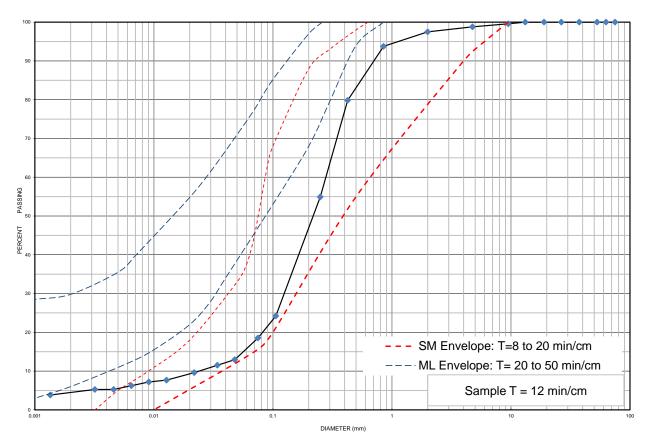
Project Number: 13237-001 Client: Koenig Developments Ltd.

Project Name: Water Balance and Hydrogeological Assessment - 245 Church St

Sample Date: Juy 21, 2021 Sampled By: Ben White - Cambium Inc.

**Location:** BH 102-21 SS 2 **Depth:** 0.6 m to 1.2 m **Lab Sample No:** S-21-0879

UNIFII	ED SOIL CLASSIF	ICATION SYSTE	М		
OLAMA OUT ( O OTS )	SAND (<4.	GRAVE	L (>4.75 mm)		
CLAY & SILT (<0.075 mm)	FINE	MEDIUM	COARSE	FINE	COARSE



	MIT SOIL CLASSIFICATION SYSTEM									
CLAY	SILT	FINE	MEDIUM	COARSE	FINE	MEDIUM	COARSE	DOLU DEDO		
CLAY	SILI	SAND				BOULDERS				

Borehole No.	Sample No.		Depth	Gravel	Sand		Silt	Clay	Moisture
BH 102-21	SS 2		0.6 m to 1.2 m	1	80		15	4	10.7
	Description		Classification	D ₆₀	D ₃₀		D ₁₀	Cu	C _c
Sand some	Silt trace Clay trace G	ravel	SM	0.275	0.130	)	0.025	11.00	2.46

Additional information availabe upon request





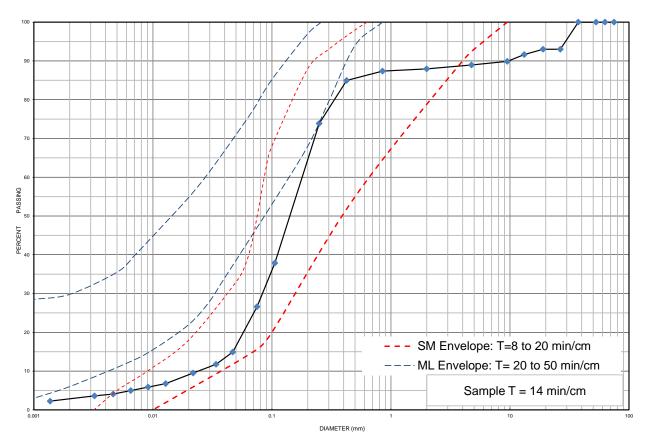
Project Number: 13237-001 Client: Koenig Developments Ltd.

Project Name: Water Balance and Hydrogeological Assessment - 245 Church St

Sample Date: July 21, 2021 Sampled By: Ben White - Cambium Inc.

**Location:** BH 102-21 SS 6 **Depth:** 4.6 m to 5 m **Lab Sample No:** S-21-0880

UNIFIED SOIL CLASSIFICATION SYSTEM								
CLAY & SILT (<0.075 mm)	SAND (<4.	75 mm to 0.075 mm)	GRAVEL (>4.75 mm)					
	FINE	MEDIUM	COARSE	FINE	COARSE			



	MIT SOIL CLASSIFICATION SYSTEM									
CLAY	SILT	FINE	MEDIUM	COARSE	FINE	MEDIUM	COARSE	DOLU DEDO		
CLAY	SILI	SAND				BOULDERS				

Borehole No.	Sample No.		Depth	Gravel	Sand		Silt	Clay	Moisture
BH 102-21	SS 6		4.6 m to 5 m	11	62		24	3	7.2
	Description		Classification	D ₆₀	D ₃₀		D ₁₀	Cu	C _c
Silty Sand	d some Gravel trace Cl	ay	SM	0.180	0.083	3	0.025	7.20	1.53

Additional information availabe upon request





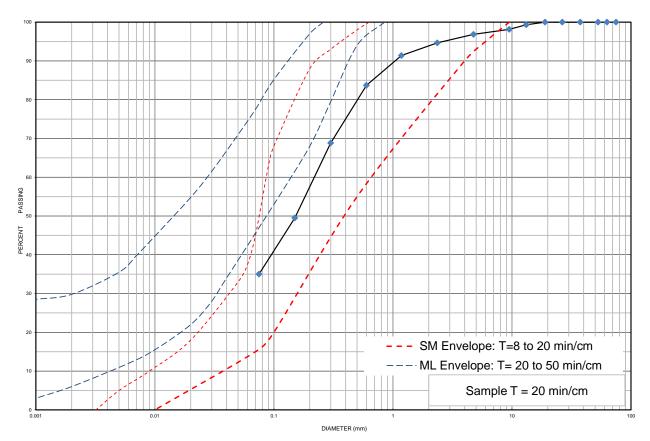
Project Number: 13237-001 Client: Koenig Developments Ltd.

Project Name: Water Balance and Hydrogeological Assessment - 245 Church St

Sample Date: July 21, 2021 Sampled By: Ben White - Cambium Inc.

**Location:** BH 103-21 SS 2 **Depth:** 0.6 m to 1.2 m **Lab Sample No:** S-21-0883

UNIFIED SOIL CLASSIFICATION SYSTEM								
CLAY & SILT (<0.075 mm)	SAND (<4.	75 mm to 0.075 mm)	GRAVEL (>4.75 mm)					
	FINE	MEDIUM	COARSE	FINE	COARSE			



	MIT SOIL CLASSIFICATION SYSTEM									
CLAY	SILT	FINE	MEDIUM	COARSE	FINE	MEDIUM	COARSE	DOLU DEDO		
CLAY	SILI	SAND				BOULDERS				

Borehole No.	Sample No.	Depth	Gravel	 Sand	Silt	Clay		Moisture
BH 103-21	SS 2	0.6 m to 1.2 m	3	62	35		16.7	
	Description	Classification	D ₆₀	D ₃₀	D ₁₀		Cu	C _c
Sand	and Silt trace Gravel	SM	0.220	-	-		-	-

Additional information availabe upon request





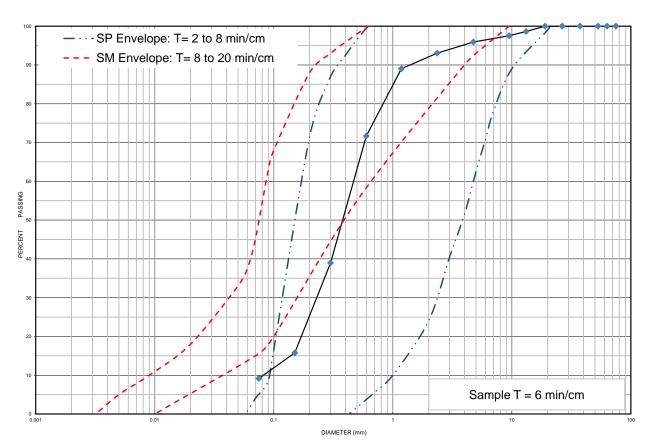
Project Number: 13237-001 Client: Koenig Developments Ltd.

Project Name: Water Balance and Hydrogeological Assessment - 245 Church St

Sample Date: July 21, 2021 Sampled By: Ben White - Cambium Inc.

**Location:** BH 104-21 SS 4 **Depth:** 2.3 m to 2.7 m **Lab Sample No:** S-21-0881

UNIFIED SOIL CLASSIFICATION SYSTEM								
CLAY & SILT (<0.075 mm)	SAND (<4.	75 mm to 0.075 mm)	GRAVEL (>4.75 mm)					
	FINE	MEDIUM	COARSE	FINE	COARSE			

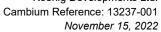


	MIT SOIL CLASSIFICATION SYSTEM									
CLAY	SH T	FINE	MEDIUM	COARSE	FINE	MEDIUM	COARSE	DOLU DEDO		
CLAY	SILT	SAND			GRAVEL			BOULDERS		

Borehole No.	Sample No.	Depth	Gravel	Sand	Silt	Clay	Moisture
BH 104-21	SS 4	2.3 m to 2.7 m	4	87	9		8.8
	Description	Classification	D ₆₀	D ₃₀	D ₁₀	C _u	C _c
Sand t	trace Silt trace Gravel	SP	0.460	0.135	0.080	5.75	0.50

Additional information available upon request







	Apı	pendix	E
<b>Thornthwaite</b>	Water	Balan	се

### Midland

	THOR	NTHWA	AITE-TY	PE MC	ONTHL	Y WAT	ER-BAI	ANCE	MODEL				
	modifie	nodified from Dingman 2001: ex. 7-13, Box 7-3 using ET model of Har								on (196	53)		
	Input D	)ata			Compu	uted Va	lues		Surplus	494	mm/y	r	
Location:	Midlar	ıd		Lat. =	44.5	degree	9	so	ILmax =	150	mm		
					0.78	rad							
Declination (deg)	-21.3	-13.3	-2.0	9.8	18.9	23.3	21.3	13.7	3.0	-9.0	-18.6	-23.3	
Declination (rad)	-0.37	-0.23	-0.03	0.17	0.33	0.41	0.37	0.24	0.05	-0.16	-0.32	-0.41	
DayLength (hr)*	9.0	10.2	11.7	13.3	14.6	15.3	15.0	13.8	12.4	10.8	9.4	8.7	
*For lat. > 66.5, replace	#NUM!	with 24	in sum	mer; 0	in winte	er.							
			N	MTMON	LY WA	TER B	ALANC	E DAT	Α				
		Temperatures in C, water-balance terms in mm.											
Month:	J	F	M	Α	M	J	L	Α	S	0	N	D	Year
	=====	=====	====	=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
P	110	70	66	65	93	90	73	78	99	90	104	104	1041
Τ	-8.5	-6.4	-1.9	5.8	12.2	18.1	20.8	19.9	15.9	9.3	3.2	-3.1	
F	0.00	0.00	0.00	0.97	1.00	1.00	1.00	1.00	1.00	1.00	0.53	0.00	
RAIN	0	0	0	63	93	90	73	78	99	90	55	0	640
SNOW	110	70	66	2	0	0	0	0	0	0	48	104	400
PACK	210	280	345	12	0	0	0	0	0	0	23	127	
MELT	0	0	0	336	12	0	0	0	0	0	26	0	373
INPUT (W _m )	0	0	0	399	104	90	73	78	99	90	81	0	1014
PET	0	0	0	41	67	101	116	102	72	41	24	0	565
W _m - PET	0	0	0	358	37	-12	-43	-24	27	49	57	0	
SOIL	150	150	150	150	150	139	104	89	116	150	150	150	
⊿ SOIL	0	0	0	0	0	-11	-35	-15	27	34	0	0	
ET	0	0	0	41	67	101	108	93	72	41	24	0	547
SURP=W-ET- ∆ SOIL	0	0	0	358	37	0	0	0	0	15	57	0	467
DEFIC=PET-ET	0	0	0	0	0	0	9	9	0	0	0	0	18



### Pre- and Post-Development Water Balance Calculations 245 Church Street, Penetanguishene, ON

### 1 Climate Information

Precipitation Actual Evapotranspiration Water Surplus	54	1 mm/yr 7 mm/yr 4 mm/yr
2 Infiltration Rates Table 2 Approach - Infiltration factors Topography: Gently Undulating Land Soil Type: predominantly sandy loam	0. 0.	_
Cover: Open Land Total Infiltration Factor	0. <b>0.</b>	
Infiltration (Water Surplus * Infiltration Factor) Run-off (Water Surplus - Infiltration)		6 mm/yr 8 mm/yr
Table 3 Approach - Typical Recharge Rates Coarse Sand and Gravel	>250	mm/yr
Fine to medium sand Silty sand to sandy silt Silt Clayey Silt Clay	200-250 150-200 125-150 100- 125 <100	mm/yr mm/yr mm/yr mm/yr mm/yr
Site development area is underlain predominantly by sar and trace clay.  Based on the above, the recharge rate is typically	nd and silty san 200-250	d with gravel mm/yr
3 Pre-Development Property Statistics Total Paved Area Total Roof Area Total Landscape Area Total	ha 0.00 0.00 5.30 5.30	m ² 0 0 53,000 53,000
4 Post-Development Property Statistics Total Paved Area Total Roof Area Total Landscape Area Total	ha 1.06 0.95 3.29 <b>5.30</b>	m ² 10,600 9,525 32,875 <b>53,000</b>



## **Pre- and Post-Development Water Balance Calculations**

245 Church Street, Penetanguishene, ON

### **5 Pre-Development Water Balance**

Land Use		Area (m²)	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run-off (m³)	
Immorrious Aroos	Paved Area	-	-	-	-	-	
Impervious Areas	Roof Area	-	-	-	-	-	
Pervious Areas	Landscape Area	53,000	55,173	28,991	18,327	7,855	
	Totals	53,000	55,173	28,991	18,327	7,855	
Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.							

### 6 Post-Development Water Balance

Land Use		Area (m²)	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run-off (m³)	
Importious Aroas	Paved Area	10,600	11,035	1,103	-	9,931	
Impervious Areas	Roof Area	9,525	9,916	992	-	8,924	
Pervious Areas	Landscape Area	32,875	34,223	17,983	11,368	4,872	
	Totals	53,000	55,173	20,078	11,368	23,727	
Assuming no infiltration occurring in paved and roof areas, and 10% of precipitation to be evaporated from paved and roof areas.							

### 7 Comparision of Pre- and Post -Development

	Precipitation (m³)	Evapotranspiration (m³)	Infiltration (m³)	Run-off (m³)
Pre-Development	55,173	28,991	18,327	7,855
Post-Development	55,173	20,078	11,368	23,727
Change in Volume	•	- 8,913	- 6,959	15,873
Change in %	•	- 31	- 38	202

### 8 Requirement for Infiltration of Roof Run-off

Volume of Pre-Development Infiltration (m³/yr)			
Volume of Post-Development Infiltration (m³/yr)	11,368		
Deficit from Pre to Post Development Infiltration (m³/yr)			
Percentage of Roof Runoff required to match the pre-development infiltration (%)			